

Florence County Government

Procurement Department

July 20, 2016

# ADDENDUM NO. 1- FRIENDFIELD FIRE STATION (BID NO. 2-16/17)

Florence County is sending to all interested firms clarification information and answers to questions concerning this Invitation to Bid. The answers are highlighted in blue and underlined. Please include this sheet with your proposal.

- 1. What is the site address? <u>The address is 2190 Hyman Road in Scranton, but it is currently</u> <u>an agricultural field.</u> <u>The parcel is on the south side of the road approximately 3000 feet</u> <u>east (0.6 miles) of the intersection of Hyman Road and Friendfield Road.</u> <u>The nearest</u> <u>residence is 2227 Hyman Road, about 200 feet west of the site.</u>
- 2. What is the height of the flagpole? <u>The flagpole is a one-piece, 33 foot pole. Specifications</u> <u>are attached.</u>
- Is 120 days correct for the fill build-out time? We are aware that it takes at least 8 weeks (60 days) for the building to arrive after the initial order, and have extended the time to 9 months (270 days).
- 4. What information can you give regarding the metal building? <u>The metal building plans are attached</u>. The design is by MESCO Building Solutions in Irving, Texas. The building as shown on the plans is MIRRORED that is, it does not match the civil plans at this time. <u>MESCO is working on the finalized plans</u>.

We will consider other metal building manufacturers, but be aware that these particular plans are already designed and match the Foundation Plan, so the delivery process will be more streamlined. If a Contractor does choose an alternate metal building company, it is their responsibility to provide and pay for modifying the building plans.

5. Do you have a Foundation Plan? <u>Yes we do, and it is attached. Like the Building Plans</u> <u>above, it is a mirror of the civil plans, and we are working on getting it corrected.</u>

- 6. Who pays for the Foundation plan? <u>Please provide a \$1,500 allowance in the bid for the</u> <u>Foundation Plan. Give it a new line on the Bid Tab.</u>
- 7. Is there a geotechnical report? Yes, it is attached.

YOU <u>MUST</u> ACKNOWLEDGE THIS ADDENDUM BY SIGNING BELOW AND SUBMITTING IT WITH YOUR BID.

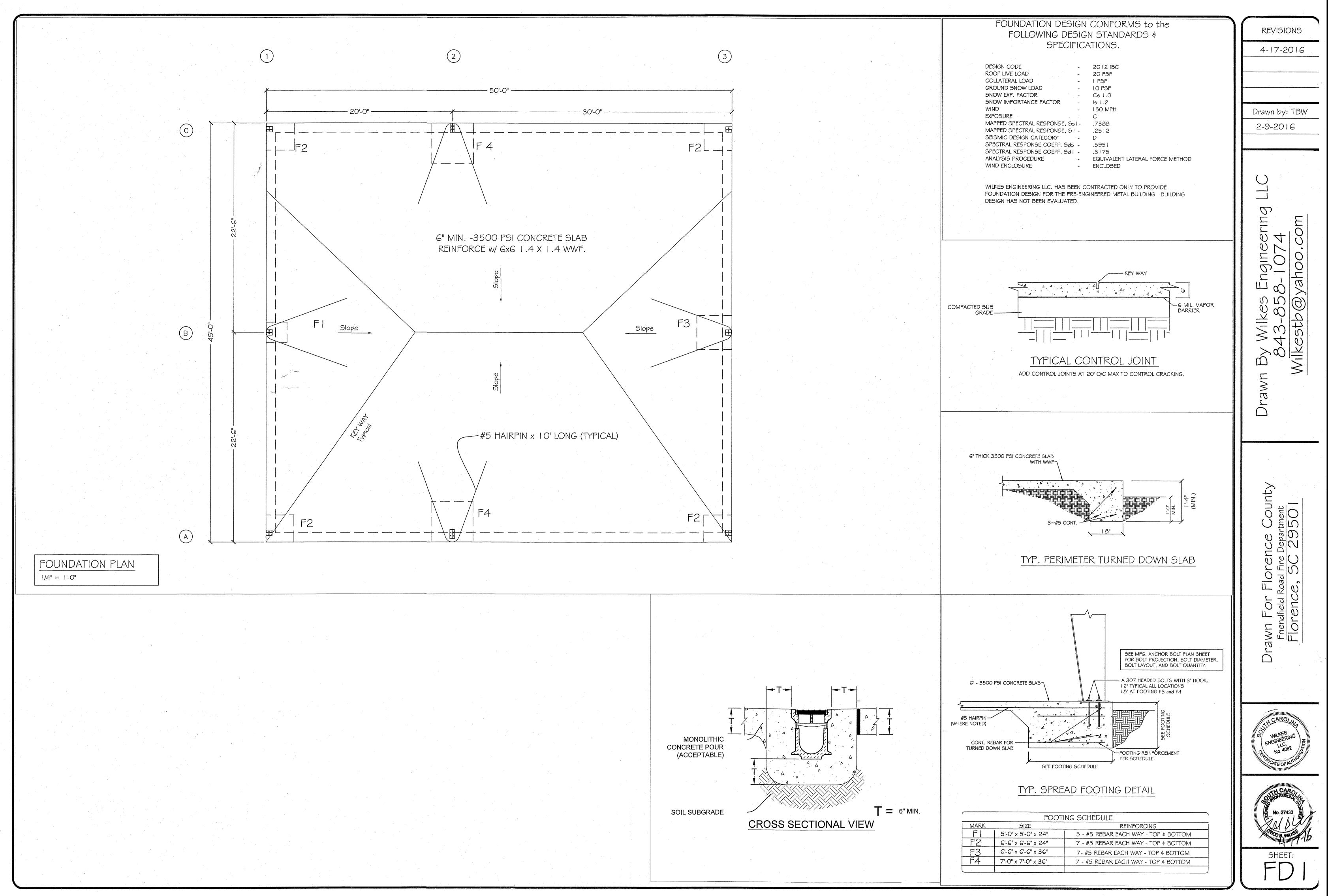
I have read and acknowledged this Addendum 1 for Bid No. 02-16/17.

Authorized Signature

Printed Name

Date

Company Name: \_\_\_\_\_



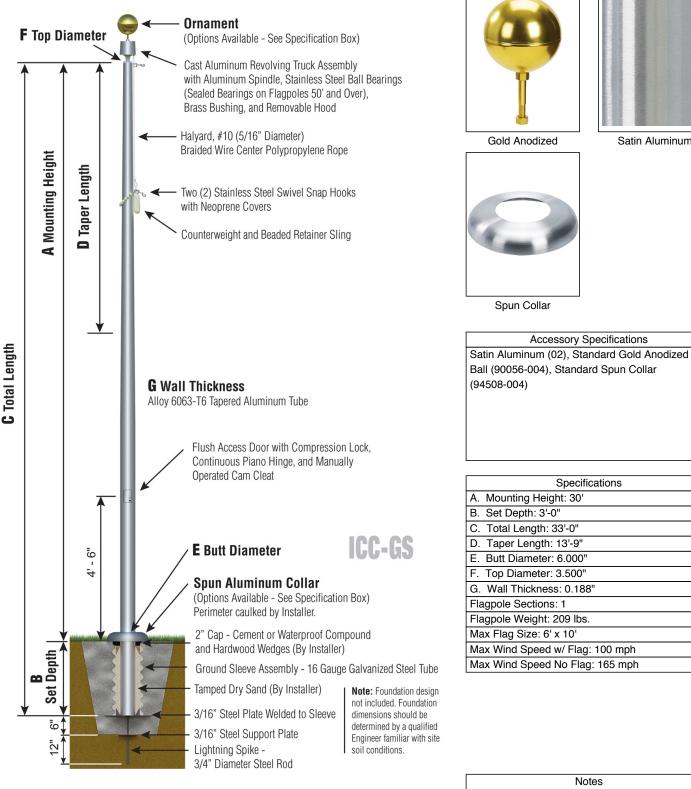
**Monarch Series - ICC** Internal Cam Cleat Rope Halyard Ground Set Installation







Satin Aluminum



10163

Customer Name:		
Dealer:		
Project:	Location:	

# REPORT OF SUBSURFACE EXPLORATION AND GEOTECHNICAL EVALUATION

HYMAN ROAD GEOTECHNICAL HYMAN ROAD FLORENCE, SOUTH CAROLINA ECS PROJECT No.: 38:1457

Prepared For FLORENCE COUNTY COMPLEX

**Prepared By** 



MAY 18, 2016



"Setting the Standard for Service"

SC Registered Engineering Firm 3240 NC Registered Engineering Firm F-1078 NC Registered Geologists Firm C-406

May 18, 2016

Ms. Wyneé Lybrand Florence County Complex 180 N. Irby St. MSC-R, Rm, B-5 Florence, SC 29501

Report of Subsurface Exploration and Geotechnical Evaluation Reference: Hyman Road Geotechnical Hyman Road Florence, South Carolina ECS Project No.: 38:1457

Dear Ms. Lybrand:

As authorized by your acceptance of our Proposal Number 38-787-P, dated April 20, 2016, ECS Carolinas, LLP (ECS) has completed the subsurface exploration and geotechnical evaluation for the proposed Hyman Road site. This report contains the results of our subsurface exploration, as well as our recommendations regarding the geotechnical design and construction aspects of the project.

We appreciate the opportunity to be of service to you during the design phase of this project and look forward to our continued involvement during the construction phase. If you have any questions concerning the information and recommendations presented in the accompanying report, or if we can be of further assistance, please do not hesitate to contact us.

Sincerely,

ECS CAROLINAS, LLP represented by;

Brenn Hay

Brennan J. Hoy, E.I. **Project Manager** 

Winslow E Goins, P.E. **Principal Engineer** South Carolina License No. 26758

William M. Porter, P.E.

**Branch Manager** South Carolina License No. 32695



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### 1.0 EXECUTIVE SUMMARY

The proposed site is an approximately 1 acre (43,560 SF) lot located on Hyman Road in Florence County, South Carolina. The lot is part of a larger property designated as TM 00290-02-007 on the Florence County Tax Map. The proposed construction will consist of a pre-fabricated metal building on a 45 x 50 feet monolithic concrete slab foundation with a 20 psf maximum live load.

Based on our review of the Site Development Plan by Aligned Engineering and the Plat prepared by Nesbitt Surveying Co., INC., the proposed finished floor elevation is 90.0 feet and current site grades range from approximately 86 to 88 feet above mean sea level. We understand the maximum proposed cut/fill is on the order of approximately 2 feet.

Hand auger borings HA-1 through HA-4 encountered approximately 8 to 10 inches of topsoil at the existing ground surface. Natural Coastal Plan soils were encountered below the surficial materials in the hand auger borings performed. The natural soils sampled in the hand auger borings generally consisted of clayey sand (SC). WDCP blow counts recorded in these soils typically ranged from 3 to 25+ blows per increment (bpi).

Relatively loose near surface soils are present on the site. As such, the near surface soils should be densified in-place by multiple passes with a large vibratory roller after clearing, grubbing, and removal of the surficial materials but prior to placement of new fill or other at-grade construction. Loose subgrade materials that cannot be adequately densified in-place will require undercutting and replacement with new engineered fill. Partial undercutting up to a depth of approximately 2 feet below existing grade along with additional densification operations may also be required.

Provided the subgrades are prepared as recommended within this report, the proposed structure can be supported on conventional shallow foundations bearing in approved natural soils or new engineered fill proportioned for a net allowable bearing pressure of 2,000 pounds per square foot (psf). Concrete slabs-on-grade supported by properly prepared subgrades may be designed using a modulus of subgrade reaction of 150 pounds per cubic inch (pci).

Specific information regarding the subsurface exploration procedures, the site and subsurface conditions at the time of our exploration, and our conclusions and recommendations concerning the geotechnical design and construction aspects of the project are discussed in detail in the subsequent sections of this report. Please note this Executive Summary is an important part of this report but should be considered a "*summary*" only and is not intended to be used exclusive of the entire report. The subsequent sections of this report constitute our findings, conclusions, and recommendations in their entirety.

### 2.0 PROJECT INFORMATION

The proposed site is an approximately 1 acre (43,560 SF) lot located on Hyman Road in Florence County, South Carolina. The lot is part of a larger property designated as TM 00290-02-007 on the Florence County Tax Map. The proposed construction will consist of a pre-fabricated metal building on a 45 x 50 feet monolithic concrete slab foundation with a 20 psf maximum live load.

Based on our review of the Site Development Plan by Aligned Engineering and the Plat prepared by Nesbitt Surveying Co., INC., the proposed finished floor elevation is 90.0 feet and current site grades range from approximately 86 to 88 feet above mean sea level. We understand the maximum proposed cut/fill is on the order of approximately 2 feet.

# 3.0 EXPLORATION PROCEDURES

# 3.1 Hand Auger Borings

Four (4) hand auger borings with associated Wildcat© Dynamic Cone Penetrometer (WDCP) testing were performed at the project site as shown on the Boring Location Plan in the Appendix. The hand auger boring logs are included in the Appendix.

Representative soil samples for hand auger borings were obtained by means of the hand operated auger sampling procedure in general accordance with ASTM Specification D-1452. In this procedure, the auger boring was made by rotating and advancing the auger bucket to the desired depths while periodically removing the bucket from the hole to clear and examine the auger cuttings.

After recovery, each sample was removed from the sampler and visually classified. Representative portions of each sample were then sealed in air tight containers and brought to our laboratory for visual classification in general accordance with the Unified Soil Classification System (USCS as described in ASTM D 2487).

In WDCP testing, a cone with a diameter of 1.47 inches is driven into the soil by a 34.94-pound hammer falling 15 inches. The number of blows required to drive the cone through 10 centimeter intervals is recorded. The blows obtained from WDCP can be correlated to Standard Penetration Test (SPT) N-values. Soil samples were not collected during the WDCP testing and the logs are included in the Appendix.

## 4.0 SITE AND SUBSURFACE CONDITIONS

## 4.1 <u>Site Observations</u>

The project site is currently farmland which is relatively flat and clear except for a partially wooded area on the east side of the site. The property is bound by Hyman Road to the north, farmland to the south and west, and a wooded area to the east.

# 4.2 Area Geology

The site is located in the Coastal Plain Physiographic Province of South Carolina. The Coastal Plain is composed of seven terraces, each representing a former level of the Atlantic Ocean. Soils in this area generally consist of sedimentary materials transported from other areas by the ocean or rivers. These deposits vary in thickness from a thin veneer along the western edge of the region to more than 10,000 feet near the coast. The sedimentary deposits of the Coastal Plain rest upon consolidated rocks similar to those underlying the Piedmont and Mountain Physiographic Provinces.

# 4.3 <u>Subsurface Conditions</u>

# 4.3.1 Soil Test Borings

**Surficial Materials:** Approximately 8 to 10 inches of topsoil was encountered at the ground surface in the hand auger borings performed.

**Natural Soils:** Natural Coastal Plan soils were encountered below the surficial materials and extended to the termination depths of the hand auger borings performed. The natural soils sampled in the hand auger borings generally consisted of clayey sand (SC). WDCP blow counts recorded in these soils typically ranged from 3 to 25+ blows per increment (bpi).

# 4.3.2 Groundwater Conditions

Groundwater was encountered within the hand auger borings at a depth of approximately 3 feet below the existing ground surface. Groundwater elevations should be expected to vary depending on seasonal fluctuations in precipitation, surface water absorption characteristics, and other factors not readily apparent at the time of our exploration.

## 5.0 CONCLUSIONS AND RECOMMENDATIONS

Based on the subsurface conditions encountered in the test borings and our experience with similar soil conditions and construction, the proposed structure can be supported on monolithic slab bearing in approved existing fill, new engineered fill, or natural soils.

## 5.1 Site and Subgrade Preparation

The first step in preparing the site for the proposed construction should be to remove existing vegetation or topsoil, and other soft, unsuitable, or deleterious material from the existing ground surface. Existing utilities that traverse the planned building area should be removed, but may remain in place in planned pavement areas. These operations should extend at least 10 feet beyond the building area and 5 feet beyond the planned pavement areas, where practical.

Relatively loose near surface soils are present on the site. As such, the near surface soils should be densified in-place by multiple passes with a large vibratory roller after clearing, grubbing, and removal of the surficial materials but prior to placement of new fill or other at-grade construction. Loose subgrade materials that cannot be adequately densified in-place will require undercutting and replacement with new engineered fill.

# Partial undercutting up to a depth of approximately 2 feet below existing grade along with additional densification operations may also be required.

The prepared subgrade should then be evaluated by an experienced geotechnical engineer or his authorized representative. The evaluation should include proofrolling the subgrade with an approved piece of equipment (such as a loaded dump truck, having an axle weight of at least 10 tons) to identify soft, loose and yielding areas. Based on the recommendations of the engineer, unsuitable materials encountered during the proofrolling operations should be repaired in-place by additional densification, or be removed and replaced with engineered fill that is placed and compacted in accordance with the recommendations of this report.

Backfill over existing utility lines warrants special attention during the subgrade evaluation. At the discretion of the geotechnical engineer, the evaluation of these areas may include test pits or hand auger borings to help assess the suitability of the soils.

The preparation of proposed building and pavement subgrades, as well as fill subgrades, should be observed on a full-time basis by a representative of ECS. These observations should be performed by an experienced geotechnical engineer, or his representative, to document that unsuitable materials have been removed and that the prepared subgrade is suitable for support of the proposed construction and/or fills.

Based on the results of the soil test borings, we expect that the soils encountered in the areas explored should generally be excavatable with conventional earth moving equipment such as pans/scrapers, loaders, bulldozers, rubber tired backhoes, etc.

# 5.2 Engineered Fill

Fill placed for support of the proposed structures and pavements, and for backfill of undercut areas and utility lines within expanded structure and pavement limits should consist of engineered fill. Engineered fill should be an approved material, free of organic matter and other deleterious materials, and have a Liquid Limit (LL) and a Plasticity Index (PI) less than 40 and 20, respectively. We also recommend that fills within structural areas have a standard Proctor (ASTM D 698) maximum dry density of at least 95 pounds per cubic foot (pcf).

Mass engineered fill placed within the building areas should be placed in lifts and moisture conditioned to within their working range of optimum moisture content, and compacted to a minimum of 95 percent of their standard Proctor maximum dry density, as determined in accordance with ASTM D 698. The upper one foot of soil supporting structures and slabs-on-grade should be compacted to a minimum of 98 percent of the maximum dry density obtained in accordance with ASTM D 698.

Similarly, isolated non-structural areas of engineered fill, such as trench line backfill, should be placed in lifts not exceeding 6 inches and moisture conditioned as mentioned above. The working range of optimum is typically within approximately 3 percent of the optimum moisture content.

On site natural soils should typically be suitable for re-use as engineered fill. Prior to the commencement of fill operations and/or utilization of off-site borrow materials, the contractor

should provide representative samples of the soil materials to ECS to assess the material's suitability for use as engineered fill, and to develop moisture-density relationships in accordance with the recommendations provided herein. Samples should be provided to the geotechnical engineer at least 3 to 5 days prior to their use to allow for the appropriate laboratory testing to be performed.

The maximum loose lift thickness depends upon the type of compaction equipment use. The table below provides maximum loose lifts that may be placed based on compaction equipment utilized.

Equipment	Maximum Loose Lift Thickness, in.
Large, Self-Propelled Equipment (CAT 815, CAT CS56, etc.)	12
Small, Self-Propelled or Remote Controlled (Rammax, etc.)	8
Hand Operated (Plate Tamps, Jumping Jacks, Wacker- Packers)	6

# LIFT THICKNESS RECOMMENDATIONS

ECS recommends that fill operations be observed and tested by an engineering technician to document that if compaction requirements are being met. The testing agency should perform a sufficient number of tests to document that compaction is being achieved. For mass grading operations we recommend a minimum of one density test per 2,500 SF per lift of fill placed or per 1 foot of fill thickness, whichever results in more tests. When dry, the majority of the site soil should provide adequate subgrade support for fill placement and construction operations. When wet, the soil may degrade quickly with disturbance from construction traffic. Good site drainage should be maintained during earthwork operations to prevent ponding water on exposed subgrades.

We recommend at least one test per 1 foot thickness of fill for every 100 linear feet of utility trench backfill. Where fill will be placed on existing slopes, we recommend that benches be cut in the existing slope to accept the new fill. Fill slopes should be overbuilt and then cut back to expose compacted material on the slope face. While compacting adjacent to below-grade walls, heavy construction equipment should maintain a horizontal distance of 1(H):1(V). If this minimum distance cannot be maintained, the compaction equipment should run perpendicular, not parallel to, the long axis of the wall.

The building areas should be well defined during fill placement by maintaining grade controls. Filling operations should be observed on a full-time basis by ECS to document that the recommended degree of compaction is achieved. The elevation and location of the in-place density tests should be accurately identified at the time of fill placement. Areas which fail to achieve the required degree of compaction should be re-compacted and re-tested until the recommended compaction is achieved. Failing test areas may require moisture adjustments or other suitable remedial activities in order to achieve the required compaction.

Fill materials should not be placed on frozen, frost-heaved or wet soils. Such materials should be removed prior to fill placement. Borrow fill materials should not contain wet or frozen materials at the time of placement. Wet or frost-heaved soils should also be removed prior to

placement of granular sub-base materials, foundation or slab concrete, and asphalt pavement materials.

If difficulties are encountered during the site grading operations, or if the actual site conditions differ from those encountered during our subsurface exploration, the geotechnical engineer should be notified immediately.

# 5.3 Foundation Design

Provided the foundation subgrades are prepared in strict accordance with the **Site and Subgrade Preparation** and **Engineered Fill sections** of this report, the proposed structure can be supported on conventional shallow foundations bearing in approved existing fill, new engineered fill, or natural Coastal Plain soils. Isolated column and continuous wall footings can be proportioned for a maximum net allowable soil bearing pressure of 2,000 pounds per square foot (psf). The net allowable soil bearing pressure refers to that pressure which may be transmitted to the foundation bearing soils in excess of the final minimum surrounding overburden pressure.

Footings should bear at a depth to provide adequate frost cover protection and develop the recommended soil bearing pressure. We recommend foundations bear at a minimum depth of 12 inches below the adjacent ground surface. To reduce the possibility of foundation bearing failure and excessive settlement due to local shear or "punching" failures, we recommend that continuous footings have a minimum width of 18 inches and isolated column footings have a minimum lateral dimension of 30 inches.

If independent shallow foundations are not desired for support of the structure, thickened turned-down edges may be incorporated into the design of the concrete slab-on-grade. The turned-down sections should extend at least 12 inches below the finished exterior grades and be at least 12 inches wide at their bearing elevation. Appropriate reinforcing steel should be incorporated into turned-down or thickened slab sections.

It is very important that the final bearing subgrades be evaluated by ECS personnel to document that the bearing soils are capable of supporting the recommended net allowable bearing pressure and suitable for construction. These evaluations should include visual observations, hand rod probing, and dynamic cone penetrometer (ASTM STP 399) testing, or other methods deemed appropriate by the geotechnical engineer at the time of construction.

Exposure to the environment may weaken the soils at the bearing elevation if the excavations remain exposed during periods of inclement weather. Therefore, foundation concrete should be placed the same day the foundations are excavated. If the bearing soils are softened by water or exposure to the environment, the softened soils must be removed from the foundation excavation bottoms prior to placement of concrete. If the excavation must remain open overnight, or if inclement weather is imminent while the bearing soils are exposed, we recommend that a 2 to 3-inch thick "mud-mat" of "lean" concrete be placed over the exposed bearing soils before the placement of reinforcing steel.

# 5.4 Floor Slab Design

Provided the slab subgrades are prepared in strict accordance with the **Site and Subgrade Preparation** and **Engineered Fill sections** of this report, a modulus of subgrade reaction value of 150 pci is appropriate. We recommend slabs-on-grade are underlain by a minimum of 4 inches of granular material having a maximum aggregate size of 1½ inches and no more than 2 percent fines. Prior to placing the granular material, the floor subgrade soil should be properly compacted, proofrolled, and free of standing water, mud and frozen soil.

A granular capillary break layer can often eliminate the need for a moisture/vapor retarder and can assist in more uniform curing of concrete. If a moisture/vapor retarder is used, special attention should be given to the surface curing of the slabs to minimize uneven drying of the slabs and associated cracking and/or slab curling. The use of a blotter or cushion layer above the vapor retarder can also be considered for project specific reasons. Please refer to ACI 302.1R96 Guide for Concrete Floor and Slab Construction and ASTM E 1643 "Standard Practice for Installation of Water Vapor Retarders Used in Contact with Earth or Granular Fill Under Concrete Slabs" for additional guidance on this issue.

We recommend that slabs-on-grade be isolated from the foundation footings so settlement of the foundations will not induce shear stresses in the floor slab. However, appropriate reinforcement should be incorporated into turned-down or thickened slab section if a monolithic slab is used. In order to reduce the crack width of shrinkage cracks that may develop near the surface of the slab, we recommend mesh reinforcement be placed in the floor slab. The Wire Reinforcement Institute recommends the mesh reinforcement be placed 2 inches below the slab surface or upper one-third of slab thickness, whichever is closer to the surface. Adequate construction joints, contraction joints and isolation joints should also be provided in the slab to reduce the impacts of cracking and shrinkage. Please refer to ACI 302.1R96 Guide for Concrete Floor and Slab Construction for additional information regarding concrete slab joint design.

# 5.5 Site Drainage

Positive drainage should be provided around the perimeter of structures to minimize the potential for moisture infiltration into the foundation and slab subgrade soils. We recommend that landscaped areas adjacent to these structures be sloped away from the construction and maintain a fall of at least 6 inches for the first 10 feet outward from the structures. Any future paved areas should also be sloped to divert surface water away from the proposed building.

The proper diversion of surface water during site grading and construction will help reduce the potential for delays associated with periods of inclement weather. Please note that the need for construction dewatering should be determined at the time of construction. If grading operations are performed during the wet seasons (i.e. fall and winter) the use of gravity flow ditches may be necessary to divert precipitation and surface water away from the construction areas. The proper diversion of surface water is especially critical since portions of the site soils are expected to be moisture sensitive. Based upon our past experience, the use of "crowning" large areas of exposed soils should be useful to help divert surface water from the prepared subgrades.

# 5.6 Construction Considerations

It is imperative to maintain good site drainage during earthwork operations to help maintain the integrity of the surface soils. The surface of the site should be kept properly graded to enhance drainage of surface water away from the proposed construction areas during the earthwork phase of this project. We recommend that surface drainage be diverted away from the proposed building areas without significantly interrupting its flow. Other practices would involve sealing the exposed soils with a smooth-drum roller at the end of the day's work to reduce the potential for infiltration of surface water into the exposed soils.

The key to minimizing disturbance problems with the soils is to have proper control of the earthwork operations. Specifically, it should be the earthwork contractor's responsibility to maintain the site soils within a workable moisture content range to obtain the required in-place density and maintain a stable subgrade. Scarifying and drying operations should be included in the contractor's price and not be considered an extra to the contract. In addition, construction equipment should not be permitted to randomly run across the site, especially once the desired final grades have been established. Construction equipment should be limited to designated lanes and areas, especially during wet periods to minimize disturbance of the site subgrades.

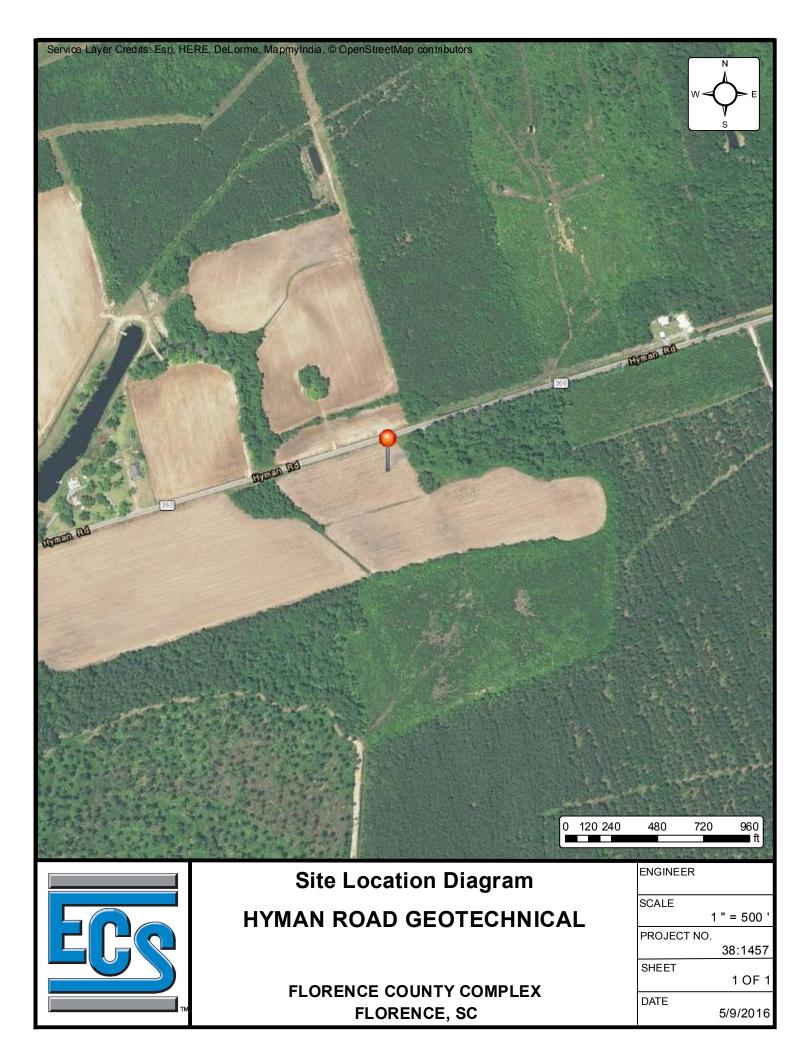
# 6.0 CLOSING

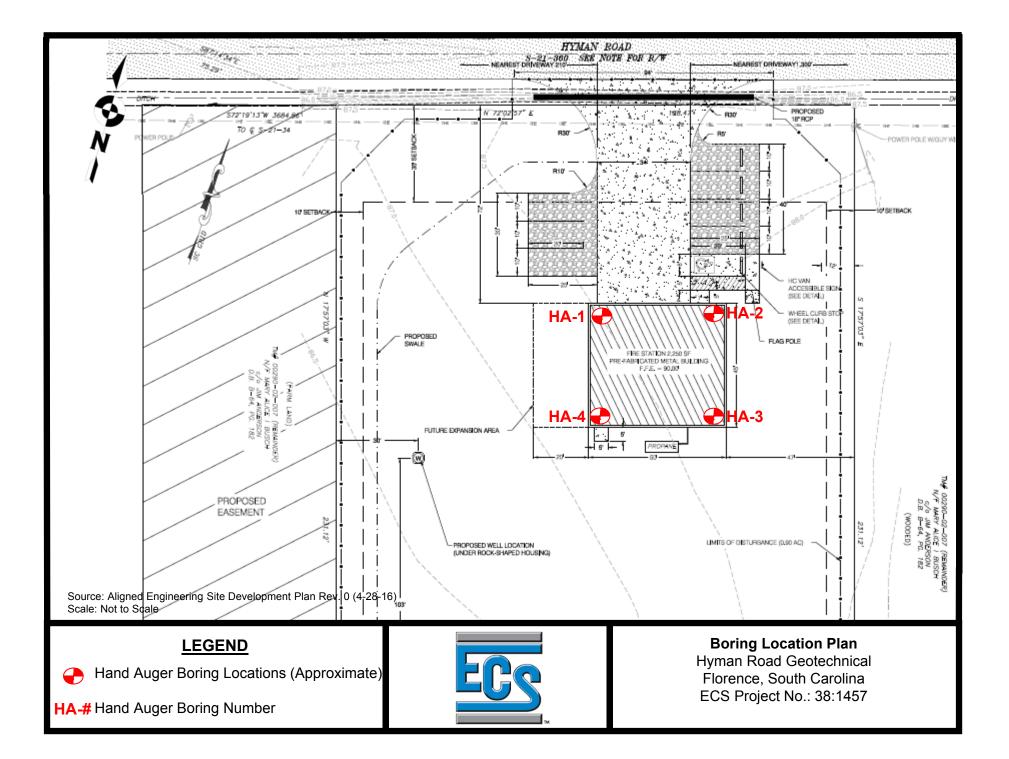
This report has been prepared in accordance with generally accepted geotechnical engineering practice. No other warranty is expressed or implied. Our evaluation of foundation support conditions is based on our understanding of the site and project information, and the data obtained in our exploration. The general subsurface conditions used in our foundation evaluation are based on interpolation of subsurface data between the borings. In evaluating the boring data, we have reviewed previous correlations between penetration resistance values and foundation bearing pressures observed in soil conditions similar to those at your site. Once the final project design criteria are established, please contact us so that our recommendations can be reviewed and modified, if necessary. The discovery of any site or subsurface conditions during construction which deviate from the data outlined in this exploration should be reported to us for our evaluation. *Furthermore, ECS should be provided a copy of the final plans and specifications in advance of construction to verify that our recommendations have been correctly interpreted.* The assessment of site environmental conditions for the presence of pollutants in the soil, rock, and groundwater of the site was beyond the scope of this exploration.

# APPENDIX

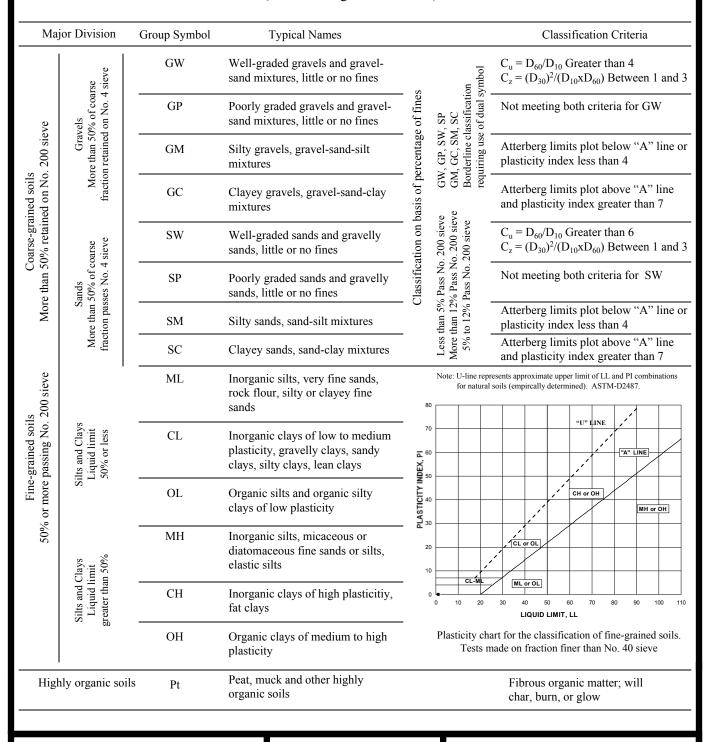
Site Location Map Boring Location Plan Unified Soil Classification System Reference Notes for Boring Logs Hand Auger Logs (HA-1 to HA-4)

Wildcat Dynamic Cone Penetrometer Logs (HA-1 to HA-4)





# Unified Soil Classification System (ASTM Designation D-2487)





UNIFIED SOIL CLASSIFICATION SYSTEM

# **REFERENCE NOTES FOR BORING LOGS**

# I. Drilling and Sampling Symbols:

SS:	Split Spoon Sampler	RB:	Rock Bit Drilling
ST:	Shelby Tube Sampler	BS:	Bulk Sample of Cutting
	Dook Corol NIX DV AV	DA.	Dower Auger (ne comp

RC: Rock Core; NX, BX, AX

- PM: Pressuremeter
- DC: Dutch Cone Penetrometer

BS: Bulk Sample of Cuttings PA: Power Auger (no sample) HSA: Hollow Stem Auger

WS: Wash Sample

Standard Penetration (Blows/Ft) refers to the blows per foot of a 140 lb. hammer falling 30 inches on a 2 inch O.D. split spoon sample, as specified in ASTM D-1586. The blow count is commonly referred to as the N value.

# II. Correlation of Penetration Resistances to Soil Properties:

Relative Density	of Cohesionless Soils	Consistency c	of Cohesive Soils
<u>SPT-N</u>	Relative Density	<u>SPT-N</u>	Consistency
0 - 4 5 - 10 11 - 30 31 - 50 51 or more	Very Loose Loose Medium Dense Dense Very Dense	0 - 2 3 - 4 5 - 8 9 - 15 16 - 30 31 - 50 50 or more	Very Soft Soft Medium Stiff Stiff Very Stiff Hard Very Hard

# III. Unified Soil Classification Symbols:

GP:	Poorly Graded Gravel	ML:	Low Plasticity Silts
GW:	Well Graded Gravel	MH:	High Plasticity Silts
GM:	Silty Gravel	CL:	Low Plasticity Clays
GC:	Clayey Gravel	CH:	High Plasticity Clays
SP:	Poorly Graded Sands	OL:	Low Plasticity Organics
SW:	Well Graded Sands	OH:	High Plasticity Organics
SM:	Silty Sands	CL - ML:	Dual Classification (Typical)
SC:	Clayey Sands		

## IV. Water Level Measurement Symbols:

WL:	Water Level	BCR:	Before Casing Removal
WS:	While Sampling	ACR:	After Casing Removal
WD:	While Drilling	WCI:	Wet Cave In
	-	DCI:	Dry Cave In

The water levels are those water levels actually measured in the borehole at the times indicated by the symbol. The measurements are relatively reliable when auguring, without adding fluids, in a granular soil. In clays and plastic silts, the accurate determination of water levels may require several days for the water level to stabilize. In such cases, additional methods of measurement are generally applied.

The elevations indicated on the boring logs should be considered approximate and were not determined using accepted surveying techniques.



PROJECT	NAME:			HAND AU	JGER #			
Hyman F	Road Geote	echnical	JOB #:	SURFAC	HA-1			
	County C	ompley		ELEVATI	ON			
DEPTH	ELEV.	LOCATION:	38:1457 ARCH./ENG:	EXCAV. EFFORT	87.5'	QP	SAMPLE	MOIST. CONT. (%)
(FT.)	(FT.)	Hyman Road, Florence, SC		EFFORT	DCP	(TSF)	NO.	(%)
0 -		DESCRIPTION C	OF MATERIAL					
0	-	Topsoil Depth [8"]						
-	-							
-	87 -							
-	-	(SC) CLAYEY SAND, Brown to Tan, N	loist to Wet					
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-	-							
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ECS REP.:		D WATER: While Drilling DATE: UNITS: □ DATE: UNITS:	EXCAVATION EFFORT: E - EASY M - ME Cave-in Depth: Groundwater		VD - VER oundwater:	Y DIFFICU	LT	
	/GC	05/06/16 Feet		Calore Drinnig. Gl	3.0'			
JB	190		I I		0.0			

PROJECT N	NAME:			HAND AL	JGER #	
Hyman R	Road Geote	echnical	JOB #:	SURFAC	HA-2	- EPa
	County C	amploy	38:1457	ELEVATI	ON	
DEPTH	County Co	LOCATION:	38:1457 	EXCAV. EFFORT	87.5'	) SAMPLE MOIST. NO. (%)
(FT.)	(FT.)	Hyman Road, Florence, SC		EFFORT	(TSF	) NO. (%)
0 -			ON OF MATERIAL			
-		Topsoil Depth [10"]				
	87 -					
-	-					
1-	-	(SC) CLAYEY SAND, Brown to Tar	n, Moist to Wet			
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-	- 50					
- 5 -	-					
- 5	-	END OF HAND AUGER @ 5.0'				
-	- 82 -					
-	02 -					
-	-					
6-	-					
-	-					
	81 –					
REMARKS:				• •	•	· ·
		$\begin{array}{l} \begin{array}{l} \begin{array}{l} \begin{array}{l} \begin{array}{l} \begin{array}{l} \begin{array}{l} \end{array} \\ \end{array} \end{array} \\ \begin{array}{l} \begin{array}{l} \end{array} \end{array} \\ \begin{array}{l} \begin{array}{l} \end{array} \end{array} \\ \end{array} \end{array} \\ \begin{array}{l} \begin{array}{l} \end{array} \end{array} \\ \end{array} \\ \begin{array}{l} \end{array} \\ \end{array} \\ \end{array} \\ \begin{array}{l} \end{array} \\ \end{array} \\ \end{array} \\ \begin{array}{l} \begin{array}{l} \end{array} \\ \end{array} \\ \end{array} \\ \end{array} \\ \end{array} \\ \begin{array}{l} \end{array} \\ \end{array} \\ \end{array} \\ \end{array} \\ \end{array} \\ \begin{array}{l} \begin{array}{l} \end{array} \\ \begin{array}{l} \begin{array}{l} \end{array} \\ \end{array} $	XIMATE BOUNDARY LINES BETWEEN SOIL TY EXCAVATION EFFORT: E - EASY M - MEL			
ECS REP.:	GNOONL	DATE: UNITS:			oundwater:	
JB/	GC	05/06/16 Feet			3.0'	

PROJECT	NAME:			HAND AU	JGER #		-	
Hyman R	Road Geote	echnical	JOB #:	SURFAC	HA-3		21	
	County Co	amplay		ELEVATI	ON			2
DEPTH	County Co	DIMPLEX LOCATION:	38:1457 ARCH./ENG:	EXCAV. EFFORT	<u>87.5'</u>	QP	SAMPLE NO.	MOIST. CONT.
(FT.)	(FT.)	Hyman Road, Florence, SC		EFFORT	DCP	(TSF)	NO.	(%)
0			N OF MATERIAL					
0-	-	Topsoil Depth [10"]						
-	-							
-	87 -							
-	-	(SC) CLAYEY SAND, Tan to Red, M	loist to Wet					
1 -	-							
-	-							
-	86 -			E			S-1	
-	-							
2 -	-							
-	-							
-	85 -							
-								
- 2_								
3 -	- -							
-	-							
-	84 -							
-	_							
4 -	-			E			S-2	
-	-							
_	83 -							
-	-							
5 —	-	END OF HAND AUGER @ 5.0'						
-								
-	82 -							
-	-							
6 -	_							
-	-							
-	81 -							
	-							
REMARKS:								-
		ATIFICATION LINES REPRESENT THE APPROX						
ECS REP.:	GROUNE	D WATER: While Drilling DATE: UNITS: UNITS:	EXCAVATION EFFORT: E - EASY M - MEL Cave-in Depth: Groundwater		VD - VER oundwater:	Y DIFFICU	LŤ	
JB/	/GC	05/06/16 Feet			3.0'			

PROJECT	VAME:			HAND AU	JGER #			
Hyman F	Road Geote	echnical	JOB #:	SURFAC	HA-4		Er	<u>)</u>
	Court C			ELEVATI	ON			
Florence DEPTH	County Co	DIMPLEX LOCATION:	38:1457 ARCH./ENG:	EXCAV	87.5'	QP	SAMPLE	MOIST.
(FT.)	(FT.)	Hyman Road, Florence, SC		EXCAV. EFFORT	DCP	(TSF)	SAMPLE NO.	MOIST. CONT. (%)
0		DESCRIPTION	OF MATERIAL					
0	-	Topsoil Depth [8"]						
-	-							
-	87 -							
-	-	(SC) CLAYEY SAND, Tan to Red, Mo	ist to Wet					
1 –	-							
-	-							
-	86 -			E			S-1	
=	-							
2 -	-							
-	-							
-	85 -							
-	-							
3 –	<u></u>							
-								
-	84 -							
-	-							
4 -	_			E				
-	-						S-2	
-	-							
-	83 -							
-	-							
5 —	-	END OF HAND AUGER @ 5.0'		<u>KAZA</u>				
-	-							
-	82 -							
-	-							
6 -								
-	-							
-	81 -							
REMARKS:	-							
	THE STR	ATIFICATION LINES REPRESENT THE APPROXIN	IATE BOUNDARY LINES BETWEEN SOIL 1	YPES. IN-SITU THE	TRANSITION	I MAY BE (	GRADUAL.	
	GROUNE	D WATER: While Drilling 🚆 After Drilling 💻 🛛	EXCAVATION EFFORT: E - EASY M - ME	DIUM D - DIFFICUL	T VD - VER			
ECS REP.:		DATE: UNITS:	Cave-in Depth: Groundwater	Before Drilling: Gr	oundwater:			
JB/	/GC	05/06/16 Feet			3.0'			

ECS Carolinas, LLP 2031 Industrial Boulevard Lexington, SC 29072

PROJECT NUMBER:	38:1457
DATE STARTED:	05-06-2016
DATE COMPLETED	05-06-2016

CREW: JB/G PROJECT: Hym ADDRESS: Hym

LOCATION: Florence, SC

<b>-</b> 1		
/GC	SURFACE ELEVATION	1:
man Road Geotechnical	WATER ON COMPLETION	J:
man Road	HAMMER WEIGHT	T: 35 lbs.
orence, SC	CONE AREA	A: 10 sq. cm

	BLOWS	RESISTANCE	GRAPH OF CONE RESISTAN	NCE		TESTED CO	NSISTENCY
DEPTH	PER 10 cm	Kg/cm <sup>2</sup>			N'	NON-COHESIVE	COHESIVE
-	8	35.5	•••••	1	10	LOOSE	STIFF
-	6	26.6	•••••	7	7	LOOSE	MEDIUM STIFF
- 1	ft 6	26.6	•••••	7	7	LOOSE	MEDIUM STIFF
-	4	17.8	•••••	4	5	LOOSE	MEDIUM STIFF
-	5	22.2	•••••	e	6	LOOSE	MEDIUM STIFF
- 2	ft 5	22.2	•••••	e	6	LOOSE	MEDIUM STIFF
-	6	26.6	•••••	7	7	LOOSE	MEDIUM STIFF
-	8	35.5	•••••	1	10	LOOSE	STIFF
- 3	ft 7	31.1	•••••	8	8	LOOSE	MEDIUM STIFF
- 1 m	6	26.6	•••••	7	7	LOOSE	MEDIUM STIFF
-	5	19.3	•••••	4	5	LOOSE	MEDIUM STIFF
- 4	ft 5	19.3	•••••	4	5	LOOSE	MEDIUM STIFF
-	7	27.0	•••••	7	7	LOOSE	MEDIUM STIFF
-	7	27.0	•••••	7	7	LOOSE	MEDIUM STIFF
- 5	ft 8	30.9	•••••	8	8	LOOSE	MEDIUM STIFF
-	11	42.5	•••••	1	12	MEDIUM DENSE	STIFF
-	12	46.3	•••••	1	13	MEDIUM DENSE	STIFF
- 6	ft 14	54.0	•••••	1	15	MEDIUM DENSE	STIFF
-	22	84.9	•••••	2	24	MEDIUM DENSE	VERY STIFF
- 2 m	24	92.6	•••••	25	5+	MEDIUM DENSE	VERY STIFF
- 7	ft 19	65.0	•••••	1	18	MEDIUM DENSE	VERY STIFF
-	21	71.8	•••••		20	MEDIUM DENSE	VERY STIFF
-	20	68.4	•••••	1	19	MEDIUM DENSE	VERY STIFF
- 8		58.1	•••••	1	16	MEDIUM DENSE	VERY STIFF
-	16	54.7	•••••		15	MEDIUM DENSE	STIFF
-	20	68.4	•••••		19	MEDIUM DENSE	VERY STIFF
- 9		65.0	•••••		18	MEDIUM DENSE	VERY STIFF
-	19	65.0	•••••		18	MEDIUM DENSE	VERY STIFF
-	20	68.4	•••••		19	MEDIUM DENSE	VERY STIFF
- 3 m 10	ft 22	75.2	•••••	2	21	MEDIUM DENSE	VERY STIFF
-							
-							
-							
- 11	ft						
-							
-							
- 12	ft						
-							
-							
- 4 m 13	ft						

HOLE #: HA-

ECS Carolinas, LLP 2031 Industrial Boulevard Lexington, SC 29072

PROJECT NUMBER:	38:1457
DATE STARTED:	05-06-2016
DATE COMPLETED:	05-06-2016

SURFACE ELEVATION:

WATER ON COMPLETION:

HAMMER WEIGHT:

CONE AREA:

HOLE #: HA-2 CREW: JB/GC PROJECT: Hyman Road Geotechnical ADDRESS: Hyman Road

LOCATION: Florence, SC

		BLOWS	RESISTANCE						TESTED CONSISTENCY		
DEP	ТН	PER 10 cm	Kg/cm <sup>2</sup>	0	50	100	150	N'	NON-COHESIVE	COHESIVE	
-		6	26.6	•••••				7	LOOSE	MEDIUM STIFF	
-		7	31.1	•••••				8	LOOSE	MEDIUM STIFF	
-	1 ft	5	22.2	•••••				6	LOOSE	MEDIUM STIFF	
-		4	17.8	•••••				5	LOOSE	MEDIUM STIFF	
-		4	17.8	•••••				5	LOOSE	MEDIUM STIFF	
-	2 ft	4	17.8	•••••				5	LOOSE	MEDIUM STIFF	
-		5	22.2	•••••				6	LOOSE	MEDIUM STIFF	
-		6	26.6	•••••				7	LOOSE	MEDIUM STIFF	
-	3 ft	5	22.2	•••••				6	LOOSE	MEDIUM STIFF	
- 1 m		5	22.2	•••••				6	LOOSE	MEDIUM STIFF	
-		6	23.2	•••••				6	LOOSE	MEDIUM STIFF	
-	4 ft	6	23.2	•••••				6	LOOSE	MEDIUM STIFF	
-		7	27.0	•••••				7	LOOSE	MEDIUM STIFF	
-		8	30.9	•••••				8	LOOSE	MEDIUM STIFF	
-	5 ft	9	34.7	•••••				9	LOOSE	STIFF	
-		9	34.7	•••••				9	LOOSE	STIFF	
-		11	42.5	•••••	••			12	MEDIUM DENSE	STIFF	
-	6 ft	16	61.8	•••••	•••••			17	MEDIUM DENSE	VERY STIFF	
-		24	92.6	•••••	•••••	••••		25 +	MEDIUM DENSE	VERY STIFF	
- 2 m		25	96.5	•••••	•••••	•••••		25 +	MEDIUM DENSE	VERY STIFF	
-	7 ft	20	68.4	•••••	•••••			19	MEDIUM DENSE	VERY STIFF	
-		20	68.4	•••••	•••••			19	MEDIUM DENSE	VERY STIFF	
-		19	65.0	•••••	•••••			18	MEDIUM DENSE	VERY STIFF	
-	8 ft	18	61.6	•••••	•••••			17	MEDIUM DENSE	VERY STIFF	
-		17	58.1	•••••	•••••			16	MEDIUM DENSE	VERY STIFF	
-		19	65.0	•••••	•••••			18	MEDIUM DENSE	VERY STIFF	
-	9 ft	18	61.6	•••••	•••••			17	MEDIUM DENSE	VERY STIFF	
-		18	61.6	•••••	•••••			17	MEDIUM DENSE	VERY STIFF	
-		19	65.0	•••••	•••••			18	MEDIUM DENSE	VERY STIFF	
- 3 m	10 ft	21	71.8	•••••	•••••			20	MEDIUM DENSE	VERY STIFF	
-											
-											
-											
-	11 ft										
-											
-											
-	12 ft										
-											
I	10.0										
- 4 m	13 ft										

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35 lbs.

10 sq. cm

ECS Carolinas, LLP 2031 Industrial Boulevard Lexington, SC 29072

PROJECT NUMBER:	38:1457
DATE STARTED:	05-06-2016
DATE COMPLETED:	05-06-2016

SURFACE ELEVATION:

WATER ON COMPLETION:

HAMMER WEIGHT:

CONE AREA:

HOLE #: HA-3 CREW: JB/GC PROJECT: Hyman Road Geotechnical ADDRESS: Hyman Road

LOCATION: Florence, SC

	BLOWS	RESISTANCE	GRAPH OF CONE	RESISTANCE		TESTED CO	NSISTENCY
DEPTH	PER 10 cm	Kg/cm <sup>2</sup>	0 50	100 150	N'	NON-COHESIVE	COHESIVE
-	6	26.6	•••••		7	LOOSE	MEDIUM STIFF
-	8	35.5	•••••		10	LOOSE	STIFF
- 1	ft 7	31.1	•••••		8	LOOSE	MEDIUM STIFF
-	5	22.2	•••••		6	LOOSE	MEDIUM STIFF
-	5	22.2	•••••		6	LOOSE	MEDIUM STIFF
- 2	ft 4	17.8	••••		5	LOOSE	MEDIUM STIFF
-	7	31.1	•••••		8	LOOSE	MEDIUM STIFF
-	7	31.1	•••••		8	LOOSE	MEDIUM STIFF
- 3	ft 6	26.6	•••••		7	LOOSE	MEDIUM STIFF
- 1 m	5	22.2	•••••		6	LOOSE	MEDIUM STIFF
-	6	23.2	•••••		6	LOOSE	MEDIUM STIFF
- 4	ft 5	19.3	•••••		5	LOOSE	MEDIUM STIFF
-	5	19.3	••••		5	LOOSE	MEDIUM STIFF
-	6	23.2	•••••		6	LOOSE	MEDIUM STIFF
- 5	ft 8	30.9	•••••		8	LOOSE	MEDIUM STIFF
-	9	34.7	•••••		9	LOOSE	STIFF
-	12	46.3	•••••		13	MEDIUM DENSE	STIFF
- 6	ft 15	57.9	•••••		16	MEDIUM DENSE	VERY STIFF
-	23	88.8	••••••		25	MEDIUM DENSE	VERY STIFF
- 2 m	22	84.9	•••••		24	MEDIUM DENSE	VERY STIFF
- 7	ft 20	68.4	•••••		19	MEDIUM DENSE	VERY STIFF
-	19	65.0	•••••		18	MEDIUM DENSE	VERY STIFF
-	20	68.4	•••••		19	MEDIUM DENSE	VERY STIFF
- 8	ft 19	65.0	•••••		18	MEDIUM DENSE	VERY STIFF
-	18	61.6	•••••		17	MEDIUM DENSE	VERY STIFF
-	20	68.4	•••••		19	MEDIUM DENSE	VERY STIFF
- 9	ft 18	61.6	•••••		17	MEDIUM DENSE	VERY STIFF
-	18	61.6	•••••		17	MEDIUM DENSE	VERY STIFF
-	19	65.0	•••••		18	MEDIUM DENSE	VERY STIFF
- 3 m 10	ft 20	68.4	•••••		19	MEDIUM DENSE	VERY STIFF
-							
-							
-							
- 11	ft						
-							
-							
- 12	ft						
-							
-							
- 4 m 13	ft						

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35 lbs.

10 sq. cm

ECS Carolinas, LLP 2031 Industrial Boulevard Lexington, SC 29072

PROJECT NUMBER:	38:1457

 DATE STARTED:
 05-06-2016

 DATE COMPLETED:
 05-06-2016

HOLE #: HA-4 CREW: JB/GC

PROJECT: Hyman Road Geotechnical ADDRESS: Hyman Road

LOCATION: Florence, SC

SURFACE ELEVATION:	
WATER ON COMPLETION:	
HAMMER WEIGHT:	35 lbs.
CONE AREA:	10 sq. cm

		BLOWS	RESISTANCE				
DEI	PTH	PER 10 cm	Kg/cm <sup>2</sup>	0 50 100 150	N'	NON-COHESIVE	COHESIVE
-		7	31.1	•••••	8	LOOSE	MEDIUM STIFF
-		6	26.6	•••••	7	LOOSE	MEDIUM STIFF
-	1 ft	4	17.8	••••	5	LOOSE	MEDIUM STIFF
-		3	13.3	•••	3	VERY LOOSE	SOFT
-		3	13.3	•••	3	VERY LOOSE	SOFT
-	2 ft	4	17.8	••••	5	LOOSE	MEDIUM STIFF
-		6	26.6	•••••	7	LOOSE	MEDIUM STIFF
-		7	31.1	•••••	8	LOOSE	MEDIUM STIFF
-	3 ft	4	17.8	••••	5	LOOSE	MEDIUM STIFF
- 1 m		4	17.8	••••	5	LOOSE	MEDIUM STIFF
-		6	23.2	•••••	6	LOOSE	MEDIUM STIFF
-	4 ft	3	11.6	•••	3	VERY LOOSE	SOFT
-		5	19.3	••••	5	LOOSE	MEDIUM STIFF
-		4	15.4	••••	4	VERY LOOSE	SOFT
-	5 ft	7	27.0	•••••	7	LOOSE	MEDIUM STIFF
-		10	38.6	•••••	11	MEDIUM DENSE	STIFF
-		11	42.5	•••••	12	MEDIUM DENSE	STIFF
-	6 ft	16	61.8	•••••	17	MEDIUM DENSE	VERY STIFF
-		25	96.5	•••••	25+	MEDIUM DENSE	VERY STIFF
- 2 m		25	96.5	•••••	25+	MEDIUM DENSE	VERY STIFF
-	7 ft	22	75.2	•••••	21	MEDIUM DENSE	VERY STIFF
-		18	61.6	•••••	17	MEDIUM DENSE	VERY STIFF
-		19	65.0	•••••	18	MEDIUM DENSE	VERY STIFF
-	8 ft	21	71.8	•••••	20	MEDIUM DENSE	VERY STIFF
-		23	78.7	•••••	22	MEDIUM DENSE	VERY STIFF
-		22	75.2	•••••	21	MEDIUM DENSE	VERY STIFF
-	9 ft	17	58.1	•••••	16	MEDIUM DENSE	VERY STIFF
-		18	61.6	•••••	17	MEDIUM DENSE	VERY STIFF
-		18	61.6	•••••	17	MEDIUM DENSE	VERY STIFF
- 3 m	10 ft	21	71.8	•••••	20	MEDIUM DENSE	VERY STIFF
-							
-							
-							
-	11 ft						
-							
-							
-	12 ft						
-							
-	10.0						
- 4 m	13 ft						

Page 1 of 1

#### BUILDER/CONTRACTOR RESPONSIBILITIES

Drawing Validity - These drawings, supporting structural calculations and design certification are based on the order documents as of the dote of these drawings. These documents describe the material supplied by the monufacturer as of the date of these drawings. Any changes to the order documents after the date on these drawings may void these drawings, supporting structural calculations and design certification. The Builder/Contractor is responsible for notifying the building authority of all changes to the order documents which result in changes to the drawings, supporting structural calculations and design certification

Builder Acceptonce of Drawings - Approval of the manufacturer's drawings and design data affirms that the manufacturer has correctly interpreted and applied the requirements of the order documents and constitutes Builder/Contractor acceptance of the manufacturer's interpretations of the order documents and standard product specifications, including its design, fabrication and quality criteria standards and tolerances. (AISC code of standard practice Sept 86 Section 4.2.1) (Mar 05 Section 4.4.1)

Code Official Approval - It is the responsibility of the Builder/Contractor to ensure that all project plans and specifications comply with the opplicable requirements of ony governing building authority. The Builder/Contractor is responsible for securing all required approvals and permits from the appropriate agency as required.

Builder is responsible for State, Federal and OSHA safety compliance - The Builder/Contractor is responsible for opplying and observing all pertinent safety rules and regulations and OSHA standards as applicable

Building Erection - The Builder/Contractor is responsible for all erection of the steel and associated work in compliance with the Metal Building Manufacturers drawings. Temporary supports, such as temporary guys, braces, false work or other elements required for erection will be determined, furnished and installed by the erector (AISC Code of Standard Practice Sept 86 Section 7.9.1) (Mar 05 Section 7.10.3)

Discreponcies - Where discrepancies exist between the Metal Building plans and plans for other trades, the Metal Building plans will govern. (AISC Code of Standard Proctice Sept 86 Section 3.3) (Mar 05 Section 3.3)

Materials by Others - All interface and compatibility of any materials not furnished by the manufacturer are the responsibility of and to be coordinated by the Builder/Contractor or A/E firm. Unless specific design criteria concerning any interface between materials if furnished as a part of the order documents, the manufacturers assumptions will govern.

Correction of Errors - Normal erection operations include the correction of minor misfits by moderate amounts of rearming, chipping, welding or cutting ond the drawing of elements into line through the use of drift pins. Errors which cannot be corrected by the foregoing means or which require major changes in the member configuration should be reported immediately to the owner and fabricator by the erector, to enable whoever is responsible either to correct the error or to approve the most efficient and economical method of correction to be used by others. (AISC Code of Standard Practice Sept 86 Section 7.12)(Mar 05 Section 7.14)

Modification of the Metal Building from Plans - The Metal Building supplied by the manufacturer has been designed according to the Building Code and specifications and the loads shown on this drawing. Modification of the building configuration, such as removing wall panels or braces, from that shown on these plans could affect the structural integrity of the building. The Metal Building Monufacturer or a Licensed Structural Engineer should be consulted prior to making any changes to the building configuration shown on these drawings. The Metal Building Manufacturer will assume no responsibility for any loads applied to the building not indicated on these drawings.

Safety Commitment — The Metal Building Manufacturer has a commitment to manufacture quality building components that can be safely eracted. However, the safety commitment and job site practices of the eractor are beyond the control of the building manufacturer. It is strongly recommended that safe working conditions and accident prevention is the top priority of any job site. Local, State and Federal safety and health standards, whether standard statutory or customary, should olwoys be followed to help ensure worker safety. Make certain all employees know the safest and most productive way to erect a building. Emergency procedures should be known to all employees. Daily meetings highlighting safety procedures are also recommended. The use of hard hats, rubber sole shoes for roof work, proper equipment for handling material, and safety nets where apolicable, are recommended. For purposes of determining lift requirements, no bundles supplied by the monufacturer will exceed 4000 lbs. For further information also reference the bill of materials for individual member weights of other structural members. If additional information is required contact the customer service department.

Foundation Design - The Metal Building Manufacturer is not responsible for the design, materials and workmanship of the foundation. Anchor rod plans prepared by the manufacturer are intended to show only location, diameter and projection of the anchor rods required to attach the Metal Building System to the foundation. It is the responsibility of the end customer to ensure that adequate provisions are made for specifying rod embedment, bearing values, tie rods and or other associated items embedded in the concrete foundation, as well as foundation design for the loads imposed by the Metal Building System, other imposed toods, and the bearing capacity of the soil and other conditions of the building site. (MBMA 06 Sections 3.2.2 (EA han

Dissimilar Materials — Never allow your roof to come in contact with, or water runoff from, any dissimilar metal including but not limited to: Copper and Arsenic Salts used in treated lumber, Calcium used in concrete, mortar and orout

Debris Removal — Any foreign debris such as sawdust, dirt, animal droppings, etc. will cause corrosion of the roof, gutters, trim, etc. if left on building surfaces for a long enough time. The roof should be periodically inspected for such conditions and if found, they should be removed

<u>Shop Primed Steel</u> — All structural members of the Metal Building System not fabricated of corrosion resistant material or protected by a corrosion resistant coating are pointed with one coat of shop primer meeting the performance requirements of SSPC Point Specification No. 15. All surfaces to receive shop primer are cleaned of oose rust, loose mill scale and other foreign matter by using, as a minimum, the hand tool cleaning method SSPC-SP2 (Steel Structures Painting Council) prior to painting. The coat of shop primer is intended to protect the steel framing for only a short period of exposure to ordinary atmospheric conditions. Shop Primed steel stored in the field pending erection should be kept free of the ground and so positioned as to minimize water-holding pockets, dust, mud and other contamination of the primer film. Repairs of damage to primed surfaces and/or removal of foreign material due to improper field storage or site conditions are not the responsibility of the manufacturer. The Manufacturer is not responsible for deterioration of the shop coat of primer or corrosion that may result from exposure to atmospheric and environmental conditions, nor the compatibility of the primer to any field opplied coating. Minor abrasions to the shop coat (including galvanizing) caused by handling, loading, shipping unloading and erection after painting or golvanizing are unavoidable. Touch-up of these minor abrasions is the responsibility of the End Customer (MBMA 06 IV 4.2.4)

### PROJECT NOTES

Material properties of steel bar, plate, and sheet used in the fabrication of built-up structural froming members conform to ASTM A529, ASTM A572, ASTM A1011 SS, or ASTM A1011 HSLAS with a minimum yield point of 50 ksi. Material properties of hot rolled structural shapes conform to ASTM A992, ASTM A529, or ASTM A572 with a minimum specified yield point of 50 ksi. Hot rolled angles, or other than flange braces, conform to ASTM 36 minimum. Hollow structural shaped conform to ASTM A500 grade b, minimum yield point is 42 ksi for round HSS and 46 ksi for rectangular HSS. Material properties of cold form light gage steel members conform to the requirements of ASTM A1011 SS Grade 55 or ASTM A1011 HSLAS Class 1 Grade 55, with a minimum yield point of 55 ksi

All bolt joints with A325 Type 1 bolts are specified as snug-tightened joints, unless noted otherwise, in accordance with the "Specification for Structural Joints using ASTM A325 or A490 bolts, June 30, 2004". Pretensioning methods, including turn-of-nut and colibrated wrench are not required unless noted otherwise.

The manufacturer does not assume any responsibility for the erection nor field supervision of the structure and or any special inspections (including inspection of the high strength bolts or field welds) as required during erection. The coordination and the costs associated for setting up and Special Inspections are the responsibility of the Erector, Owner, Architect, or Engineer of Record.

Design is based upon the more severe loading of either the roof snow load or the roof live load.

Loads, as noted, are given within order documents and are applied in general accordance with the applicable provisions of the model code and/or specification indicated. Neither the monufacture nor the certifying engineer declares or attests that the loads as designated are proper for the local provisions that may apply or for site specific parameters. The manufacturer's Engineer's certification is limited to design loads supplied by an Architect and/or engineer of record for the overall construction project,

This project is designed using manufacture's standard serviceability standards. Generally this means that all stresses and deflections are within typical performance limits for normal occupancy and standard metal building products. If special requirements for deflections and vibrations must be adhered to, then they must be clearly stated in the contract documents.

X-bracing (if applicable) is to be installed to a taut condition with all slack removed. Do not lighten beyond this state

The design collateral load has been uniformly applied to the design of the building. Hanging loads are to be attached to the purlin web. This may not be oppropriate for heavily concentrated loads. Any attached load in excess of 150 pounds shall be accounted for by special design performed by a licensed engineer using concentrated loads and may require separate support members within the roof system.

This metal building system is designed as enclosed. All exterior components (i.e. doors, windows, vents, etc.) must be designed to withstand the specified wind looding for the design of components and cladding in accordance with the specified building code. Doors are to be closed when a maximum of 50% of design wind velocity is reached.

#### DESIG THIS STRUCTURE IS INDICATED AND

THE BUILDER IS TO C

FRAME / ROOF DEAD

COLLATERAL (LIGHTS

FRAME / ROOF LIVE

RISK CATEGORY

SNOW LOAD GROUND SNOW LOA

> SNOW LOAD IMPORT FLAT ROOF SNOW 1

SNOW EXPOSURE F THERMAL FACTOR (

WIND LOAD

ULTIMATE WIND SPE WIND EXPOSURE CA

TOPOGRAPHICAL FAC

INTERNAL PRESSURE

ZONE 4, COMPONEN 46.532 PSF

ZONE 5, COMPONEN 46.532 PSF

ZONES PER ASCE RAIN INTENSITY 5-MINUTE DURATIC RECURRENCE (11)

5-MINUTE DURATIO RECURRENCE (12)

SEISMIC LOAD Ss\_0.7388\_

1.50 \_\_\_\_ SEISMIC IMPORTANCE FACTOR (le) S<sub>De</sub> 0.59<u>51</u> S1 0.2512 S<sub>01</sub> 0.3176 D \_\_\_\_ SITE CLASS D SFISMIC DESIGN CATEGOR

BASIC FORCE RESISTING SYSTEM RESPONSE MODIFICATION COEFFIC SYSTEM OVER-STRENGTS FACTOR

SEISMIC RESPONSE COEFFICIENT( BLDG DESIGN BASE SHEAR (V)

THE TRANSVERSE DIRECT

	BASIC FORCE RESISTING SYSTEM*
C4.	STEEL ORDINARY MOMENT FRAME
83,	STEEL ORDINARY CONCENTRIC BRACED FRAMES
н.	STRUCTURAL STEEL SYSTEMS NOT SPECIFICALLY
	DETAILED FOR SEISMIC RESISTANCE
G2.	Inverted pendulum systems
	CANTILEVERED COLUMN SYSTEMS

### BUILDING SIZE: 45'-0"

ISSUE	ÐATE	DESCRIPTION	BY	СК'0	DSN			MES	^R	uilding	Solutions		
A	11/20/15	FOR CONSTRUCTION PERMIT	PNR	PNR	MGS			MED		anung	Joranons		
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				-		Building	Solutions	Voice 214	1-687-9	999 Fax	214–687 <u>–9737</u>		
						PROJECT:	Fleming Town	Fire					
						CUSTOMER:	ACE CONSTRUC	TION CO., INC	-	OWNER	FLORENCE COUNTY	-	
		· · ·		1	<u> </u>	LOCATION:	Pamplico, SC	29583,					
						CAD	DATE	SCALE	PHASE	BUILDING ID	JO8 NUMBER	SHEET NUMBER	
		·					11/20/15	N.T.S.	1	A	15-B-17264	C1	

Rev. 8/12/14

IN LOADI Designed utilizin Lied as required BC 12	ig the loads
onfirm that thes its of the local	E LOADS COMPLY BUILDING DEPARTMENT
D LOAD	2.730 PSF
->	1 PSF
5)	Par
LOAD	12 /20.00 PSF
	<u>IV Pos</u> t
ው (Pg)	10.000 PSF
TANCE FACTOR (1s)	1.2000
.OAD (Pf)	12 PSF
ACTOR (Ce)	1.0
CI)	1.00
ED	<u>150</u> MPH
TEGORY	С
TOR	1.0
COEFFICIENT (GC)	pi) 0.18 /-0.18
√T WIND LOAD ≤ 1	OFT <sup>2</sup>
PRESSURE -50.40	9 PSF SUCTION
NT WIND LOAD < 1	OFT <sup>2</sup>
PRESSURE -61.92	6 PSF SUCTION
7-10; FIG. 30.4-1 SHOWN ARE UN-F	ACTORED
IN. 5-YEAR	.0000 IN/HOUR
N 25-YEAR	1.0000 IN/HOUR
	1.0000 IN/ DOOR

ANALYSIS PROCEDURE: EQUIVALENT LATERAL FORCE

Т	RANSVERSE	LONGITU FRONT	IDINAL BACK
	C4	G2	83
HENT(R)	3.25	1.25	3.25
(Ω <sub>0</sub> )	3.0000	1.2500	2.0000
- C")	0.275	0.715	0.275
		9.17	_(k)
ION IS I	PARALLEL TO T	HE RIGID FRA	MES .

THE LONGITUDINAL DIRECTION IS PERPENDICULAR TO THE RIGID FRAMES

x 50'-0" x	14'-3" × 18'-0"
lutions	
TX 75061	Mema

Α

	*DRAW	ING INDEX
ISSUE	PAGE	DESCRIPTION
A	C1	COVER SHEET
0	۶î	ANCHOR BOLT PLAN
0	F2	ANCHOR BOLT REACTIONS
0	F3	ANCHOR BOLT DETAILS
A	E1	ROOF FRAMING PLAN
A	E2	ROOF SHEETING PLAN
A	E3	FRONT SIDEWALL
A	E4	BACK SIDEWALL
A	E5	LEFT ENDWALL .
A	E6	RIGHT ENDWALL
A	E7	FRAME CROSS SECTION
A	EB	WALL LINEAR
A	DET1~15	STANDARD DETAILS

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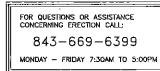
# DRAWING STATUS

#### FOR APPROVAL

THESE DRAWINGS, BEING FOR APPROVAL, ARE BY DEFINITION NOT FINAL AND ARE FOR CONCEPTUAL REPRESENTATION ONLY. THEIR PURPOSE IS TO CONFIRM PROPER INTERPRETATION OF THE PROJECT DOCUMENTS. ONLY DRAWINGS ISSUED "FOR ERECTOR INSTALLATION" CAN BE CONSIDERED AS COMPLETE.

X FOR CONSTRUCTION PERMIT THESE DRAWINGS, BEING FOR PERMIT, ARE BY DEFINITION NOT FINAL ONLY DRAWINGS ISSUED "FOR ERECTOR INSTALLATION" CAN BE CONSIDERED AS COMPLETE.

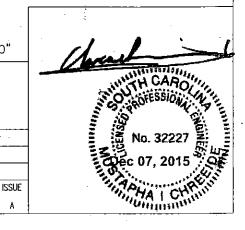
### FOR ERECTOR INSTALLATION FINAL DRAWINGS FOR CONSTRUCTION.

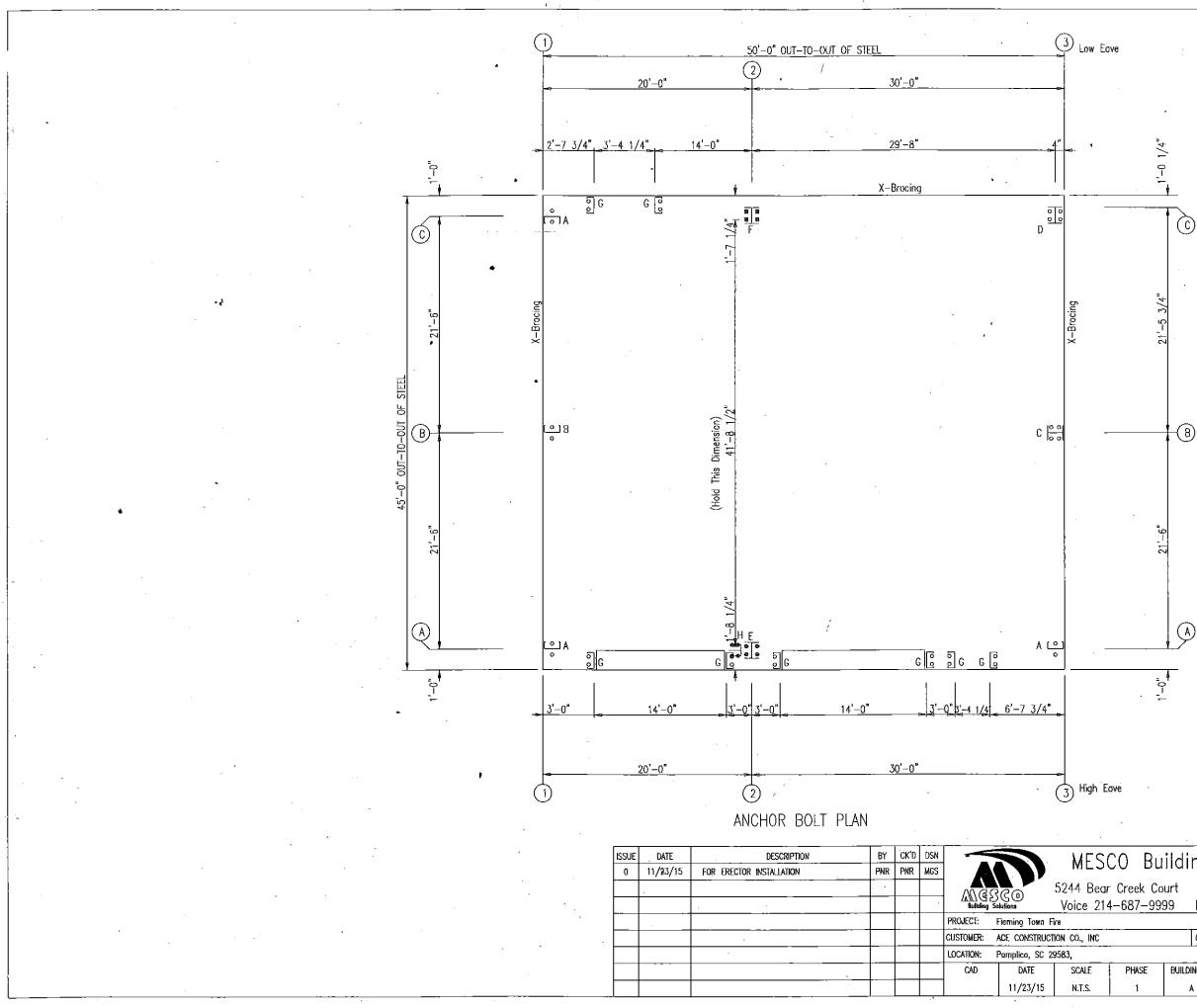


ENGINEERING SEAL

THIS CERTIFICATION COVERS PARTS MANUFACTURED AND DELIVERED BY THE MANUFACTURER ONLY, AND EXCLUDES PARTS SUCH AS DOORS, WINDOWS, FOUNDATION DESIGN AND ERECTION OF THE BUILDING

THESE DRAWINGS AND THE METAL BUILDING SYSTEM THEY REPRESENT ARE THE PRODUCT OF AN AFFILIATE OF NCI GROUP, INC. - 10943 N. SAM HOUSTON PARKWAY W., HOUSTON, TX 77064, THE PROFESSIONAL ENGINEER WHOSE SEAL APPEARS HEREON IS EMPLOYED BY AN AFFILIATE OF NCI GROUP, INC. AND IS NOT THE ENGINEER-OF-RECORD FOR THE OVERALL PROJECT.





O Dio= 5/8"
 ∞ Dio= 3/4"
 ⊕ Dio=1"

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ding	Solutions			HUILDH C	ARO	
	ving, TX 75061	Mema		S STROFES	SIONAL	
	214-687-9737		turjee	No. 3	2227	(IIII)
OWNER	: FLORENCE COUNTY	÷	1111	Qec 07,	2015	
BUILDING ID	JOB NUMBER	SHEET NUMBER	ISSUE	"IN AP	CHERN	
A	15-B-17264	F1	o	14 th 11	manne	

#### RAME LINES: BUILDING BRACING REACTIONS ENDWALL COLUMN: ANCHOR BOLTS & BASE PLATES $\odot$ Base\_Plate (in) Width Length Grout (in) Reactions in plane of woll ± Reactions (k ) —Wind --- - Seismic — Anc.\_Bolt Qty Dio Frm Line " Ponel\_Shear (16/il) Wind Seis Thick - Col Line — Wall Loc " Une Horz Vert Harz Vert 2 0.625 7.000 12.00 0.250 0.0 C 12.00 12.00 12.00 12.00 12.00 2 0.625 2 0.625 2 0.625 2 0.625 4 0.625 7.000 7.000 7.000 7.000 6,000 0,250 0.0 L\_EW F\_SW R\_EW B\_SW C,B Bracing 0.250 0.250 0,375 0.0 0.0 0.0 B,C 3,2 EW reaction: 2.3 3 C 3 В 4 0.625 5.000 0.375 0.0 C (a)Wind column at colu NOTES FOR REACTIONS \*See RF reactions loble (or vertical and horizontal reactions in plane of the rigid frame Building reactions are based on The following building data: WIDTH (FT) EAVE HIGHT (FT) COLAFERAL LOAD (psf) ROOF SLOW LOAD (psf) ROOF SLOW LOAD (psf) ROOF SLOW LOAD (psf) ROOF SLOW LOAD (psf) RWHO SPEED (UPH) WHO SCORE CLOSED/OPEN LIPORTANCE - WIND IMPORTANCE - WIND SEDSING ZONE = 45 = 50 = 14.25 / 18 = 1.0:12 / = 2.730 = 12 = 12 = 12 = 12 = 12 = 12 = 150 = 150 = Closed = 1.50 = D WIND COLUMN REACTIONS Loc Line Line R/L Lood\_ID F\_SW A 2 Reactions Vert (k ) Anc\_Bolt Qity Dia 8ose\_Plote(in) Length Morrient (f—k ) Horz (k ) Width Thick 115,8 115,9 8.000 0,750 77.2 77.3 8.000 6.8 6,8 4 1.000 RIGID FRAME: VI TI V Frm Line Col Line 2 C 2 A RIGID FRAME: Frame Colums Line Line 2 C 2 Å Courrs Line C Å Horiz 1.0 -1.0 ANCHOR BOLT SUMMARY Proj (in) 2.00 2.00 2.50 3.00 Dia (in) Frame Column Une Une 2 C 2 A Туре Qty Locate 5/8 5/8 3/4 1 F1554 F1554 F1554 F1554 O 16 O 16 ⊠3 4 ⊕ 4 ⊕ 4 Jornb Endwall Frame Frame WindCol Note Frome Column Line Line 2 C vertical rection are included in

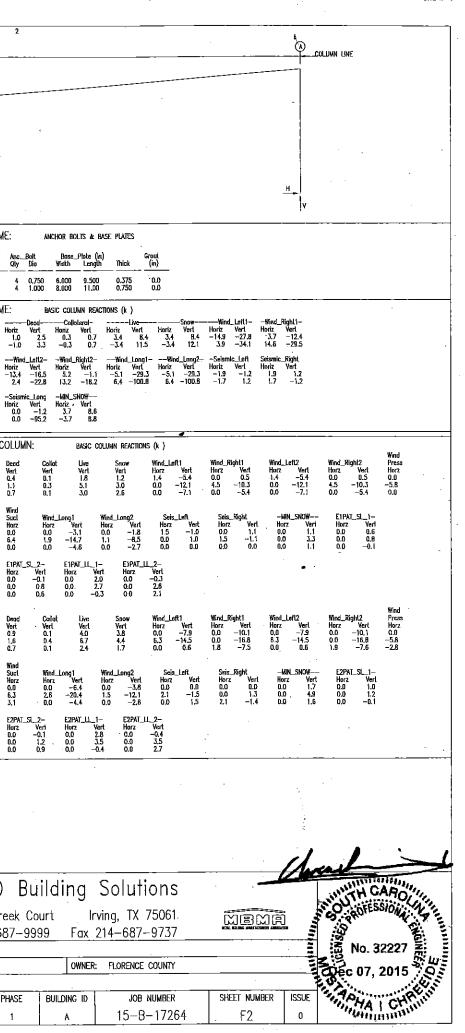
### rigid frame reactions

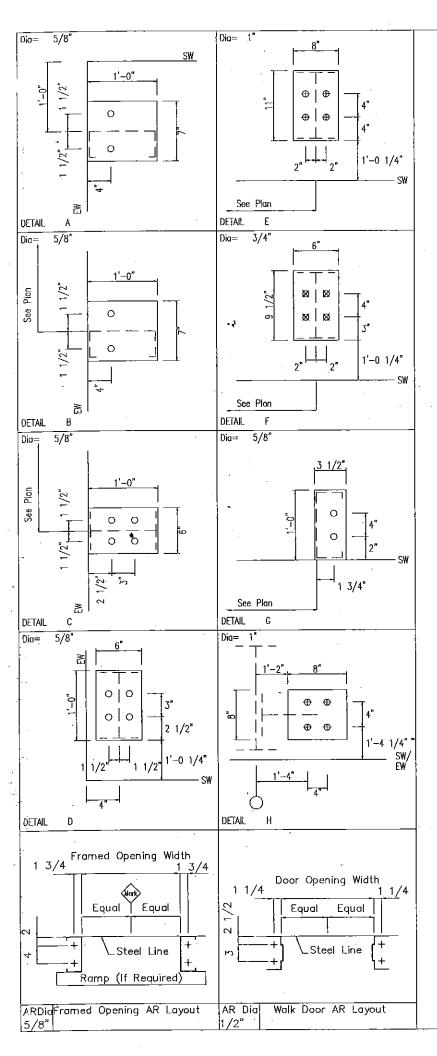
		2	ž	0.0	_9
	GENERAL NOTES	2	٨	0,0	-9
	1. THE REACTIONS PROVIDED ARE BASED ON THE ORDER DOCUMENTS	END	WALL	COLUM	N:
	AT THE TIME OF MAALING, ANY CHANGES TO BUILDING LOADS OR DIMENSIONS MAY CHANGE THE REACTIONS. THE REACTIONS	Frm	Col Line	Deod Vert	
	WILL BE SUPERSEDED AND VOIDED BY ANY FUTURE WAILING. 2. REACTIONS ARE PROVIDED AS UN-FACTORED FOR EACH LOAD GROUP APPLIED TO THE COLUMN. THE FOUNDATION ENGINEER		CB	0.4	
	WILL APPLY THE APPROPRIATE LOAD FACTORS AND COMBINE THE REACTIONS IN ACCORDANCE WITH THE BUILDING CODE AND	i	Ä	0.7	
	DESIGN SPECIFICATIONS TO DEFERMINE BEARING PRESSURES AND CONCRETE DESIGN. THE FACTORS APPLIED TO LOAD GROUPS	Frm	Col	Wind Sucl	
	For the steel column design may be different than the factors used in the foundation design.	Une 1	Line C	Horz D.C	
	3. THE MANUFACTURER DOES NOT PROVIDE "MAXIMUM" LDAD COMBINATION REACTIONS, HOWEVER, THE MOMOUAL LDAD		Ð	6. <del>4</del> 0.0	
	Reactions provided way be used by the foundation enganeer to determine the applicable load combinations for his/her design procedures and allow for an economical foundation	. Em	Col	E1PAT_	5
	DESIGN 4. THE METAL BUILDING MANUFACTURER IS RESPONSIBLE FOR THE	Lirve	Line C	Horz 0.0	-
	DESIGN OF THE ANCHOR BOLT DIAMETER ONLY TO PERMIT THE TRANSFER OF FORCES BETWEEN THE BASE PLATE AND THE		8	0,0 0.0	ĺ
	ANCHOR BOLT IN SHEAR, BEARING AND TENSION, BUT IS NOT RESPONSIBLE FOR THE ANCHOR BOLL EMBEDMENT FOR TRANSFER	<b>5</b>	<b>C-I</b>	Dead	•
	OF FORCES TO THE FOUNDATION, THE METAL BUILDING MANUFACTURER DOES NOT OCSIGN AND IS NOT RESPONSIBLE FOR THE DEFINITION AND CONFIDENTIAL OF THE FORMULATION	Frm Line 3	Col Line Å	Dead Vert 0.9	
	THE DESIGN, MATERIAL AND CONSTRUCTION OF THE FOUNDATION Embedwents, the END use customer should assure himself that adequare provisions are made in the foundation	33	BC	1.6 0.7	
1	DESIGN FOR LOADS MPOSED BY COLUMN REACTIONS OF THE BUILDING, OTHER IMPOSED LOADS, AND BEARING CAPACITY OF			Wind	
• •	The soil and other conditions of the building site. It is recommended that the anchorage and foundation of	Frm Line	Col Line	Suct Horz	
	THE BUILDING BE DESIGNED BY A REGISTERED PROFESSIONAL EXCINER EXPERIENCED IN THE DESIGN OF SUCH STRUCTURES,	3	B	0.0 6.3	
	(SECTION A3 MBHA 2005 METAL BUILDING SYSTEMS MANUAL) 5. BOTTOM OF ALL BASE PLATES ARE AT THE SAME ELEVATION, (UNLESS NOTED)	3	C	3.1	_
	6, ANCHOR RODS ARE ASTM F1554 GRADE 36 MATERIAL UNLESS NOTED OTHERWISE.	Frm Line 3	Col Line	E2PAT_ Horz 0.0	.SL_1
		3	·A	0.0	-

Col Line A B C Frm Line 3 3 3 3

ISSUE	DATE	DESCRIPTION	BY	CK D	DSN	MESCO Build
0	11/23/15	FOR ERECTOR INSTALLATION	PNR	PNR	MGS	
		·				5244 Bear Creek Court
	·	· · · · · · · · · · · · · · · · · · ·	-	1		Building Solutions Voice 214–687–9999
					ļ	PROJECT: Fleming Town Fire
					1	CUSTOMER: ACE CONSTRUCTION CO., INC
	-	· · · ·				LOCATION: Pomplico, SC 29583,
			1			CAD DATE SCALE PHASE BU
	-		<u> </u>			11/23/15 N.T.S. 1

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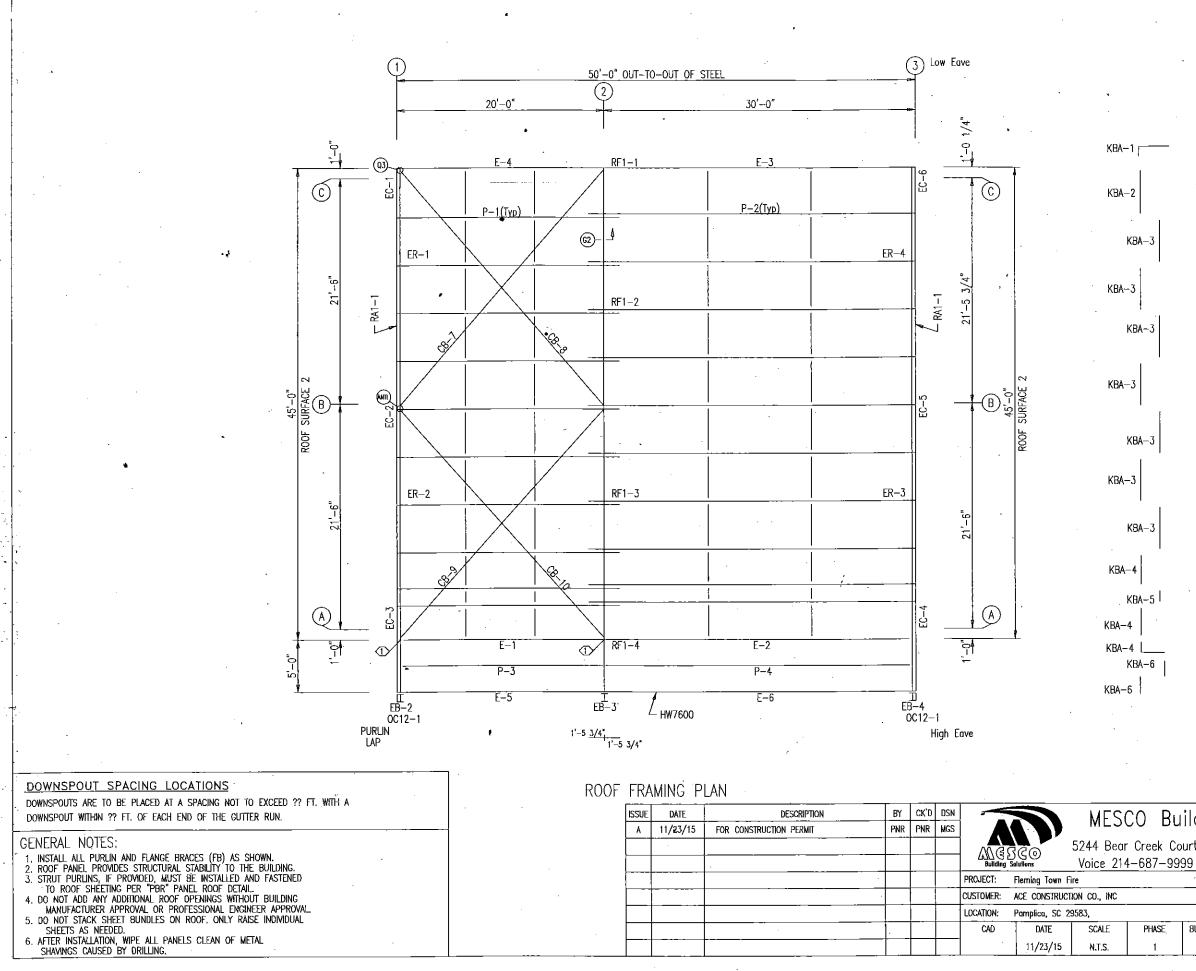




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		<u> </u>						PROJECT:	Reming Town	Fire			
								CUSTOMER:	ACE CONSTRUC	ction co., inc			
		· - ·			-			LOCATION:	Pamplica, SC	29583,			
								CAD	DATE	SCALE	PHAS	É	Bl
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Fax 2	14-687-97 <u>37</u>			NSE.	
OWNER:	FLORENCE COUNTY			B No. 3222	
L OHINER.				Dec 07, 201	
UILDING ID	JOB NUMBER	SHEET NUME	BER (SSUE	APHATCY	RUIN
	15-B-17264				



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EXTENSION	V/CAI	NOPA B	ioĻīs			
MARK	<u>N</u>		QUAN	TYPE	DIA	LENGTH
EB-2/C	<b>B</b> S37:	5	4	A325	1/2"	1 3/4"
EB-3/C	BS37:	5	8	A325	1/2 <b>"</b> 1/2"	1 3/4"
EB4/C	8537	5	4	<u>A325</u>	<u>1/2"</u>	1 3/4"
SPECIA						
ROOF	PLAN			511		WACH
		QUAN 2	TYPE A325	DIA 1/2"	<u>LENGTH</u> 1 1/4"	WASH 2
						· · · · · - ·
		/BER T/ )F PLAI				
	MAF		PART		LENGTH	
	001		0C1214		8'-9 1/1	6″
	EB- EB-	- 1	₩12X14 ₩12X14		6'-10 11 6'-10 11	/16" /16"
	EB-		W12X14		6'-10 11	/16"
	P-		12X35Z	13	21'-5-1/	'2 <b>"</b>
	P-		12X35Z		31'-5 1/ 19'-0"	2"
	Р- Р-	-3	12X35Z 12X35Z		19 -0 29'-0"	
	E-		12ES1H		19'-0"	
	E-		12ES1H		29 -0	
	E-		12ES1L		29'-11 1	/2
	E- E-		12ES1L 12X35C		19'-11 1 19'-11 1 29'-11 1	/2" /2"
	Ē-		12X35C	14	29-11 1	//2" /2"
	CB-		1/2" D	A. ROD	29'-3"	
	CB-			A. ROD	29'-6" 28'-10"	
-	CB-		1/2 0	a. Rod A. Rod	28'-8"	
	KB/		່ ບໍ່າ້ໍ້າ້ຳກຳ		1-0 5/1	6"
	KB/		L1X1X1		1'-0 5/1 4'-6"	
	KB/   KB/		L1X1X1-		4'-9" 3'7"	
	KD/		L1X1X1		1'-10 1/	′8″ .
	KB/		LIXIXI		2'-8 1/4	

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	ving, TX 75061 214–687–9737			SO ROFES	SIONAC A T	
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OWNER	FLORENCE COUNTY			Qec 07,	2015	Ξ
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UILDING ID	JOB NUMBER	SHEET NUMBER	ISSUE	1, PHA	CHREIN	
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(2) 30'-0" 20'-0" -0-1-1 .  $\bigcirc$ 21'-6" 2 45'-0" SURFACE 50'-9 1/2" • ROOF 21'-6"  $\bigcirc$ **0** "0" "1" "10" ~

- /-

(1)

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50'-0" OUT-TO-OUT OF STEEL

ROOF SHEETING PLAN PANELS: 24 Ga. DOUBLE—LOK — Galvalume [A] SOFFIT PANELS: 26 Ga. PU — TBD

ISSUE	DATE	DESCRIPTION	BY	ск'р	dsņ			MES	CO Bi	iildi
A	11/23/15	FOR CONSTRUCTION PERMIT	PNR	PNR	MGS					inui
							360	5244 Bear	<sup>-</sup> Creek C	ourt
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						PROJECT:	Fleming Town	Fire		
	-					CUSTOMER:	ACE CONSTRUC	TION CO., INC		
· 1						LOCATION:	Pamplica, SC	29583,		
						CAD	DATE	SCALE	PHASE	BUILD
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21'-6"

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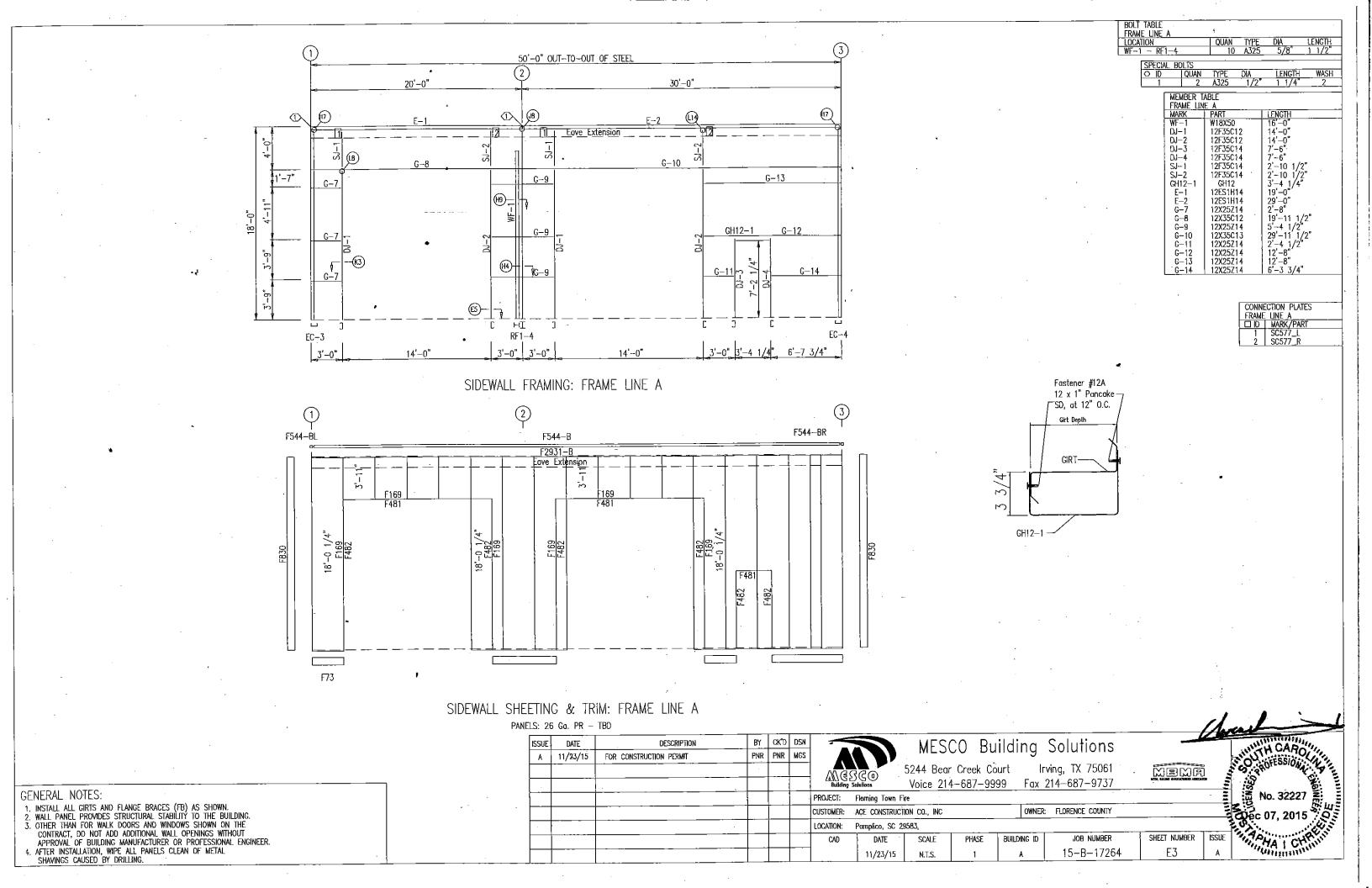
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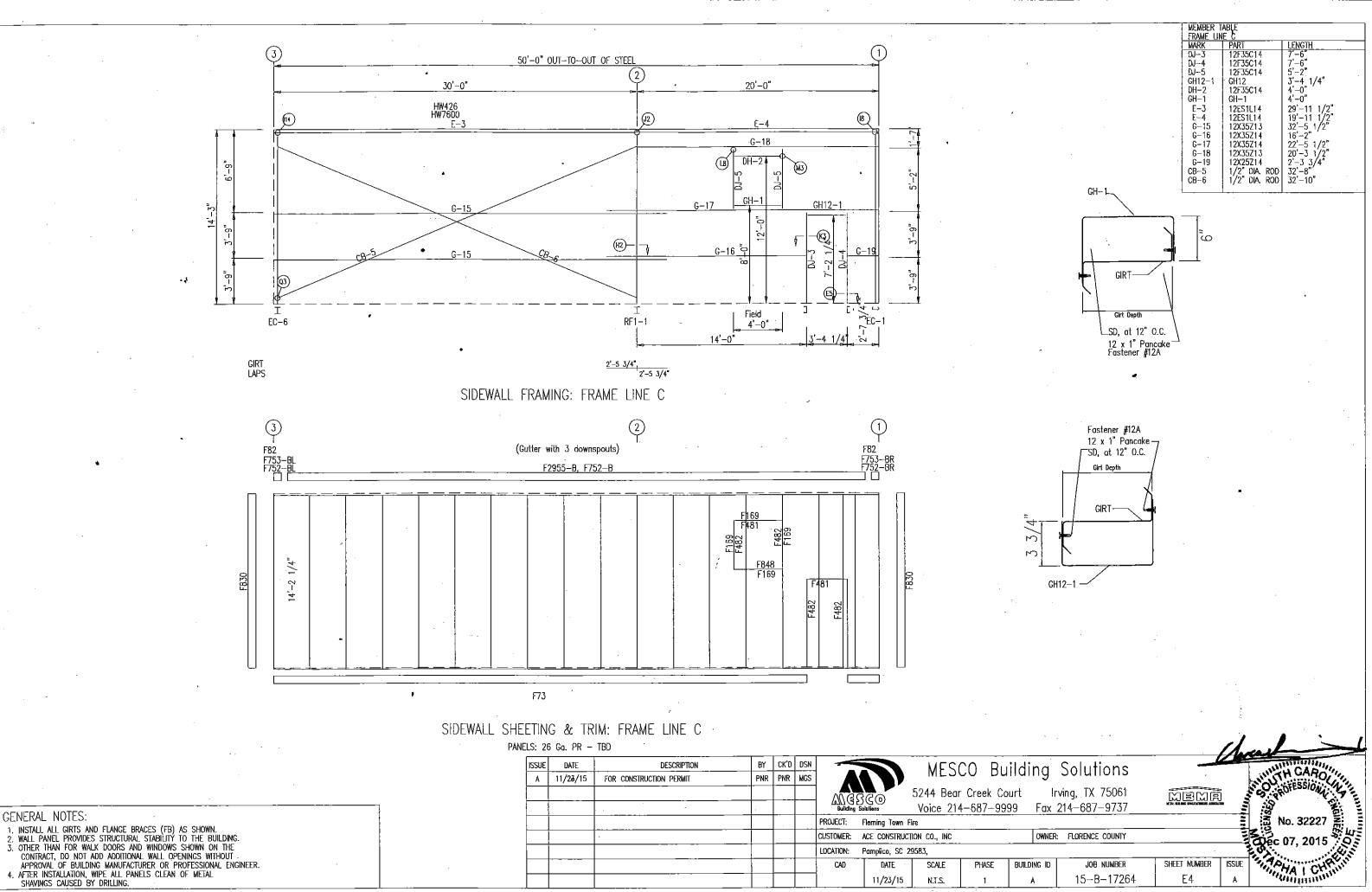
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ROG

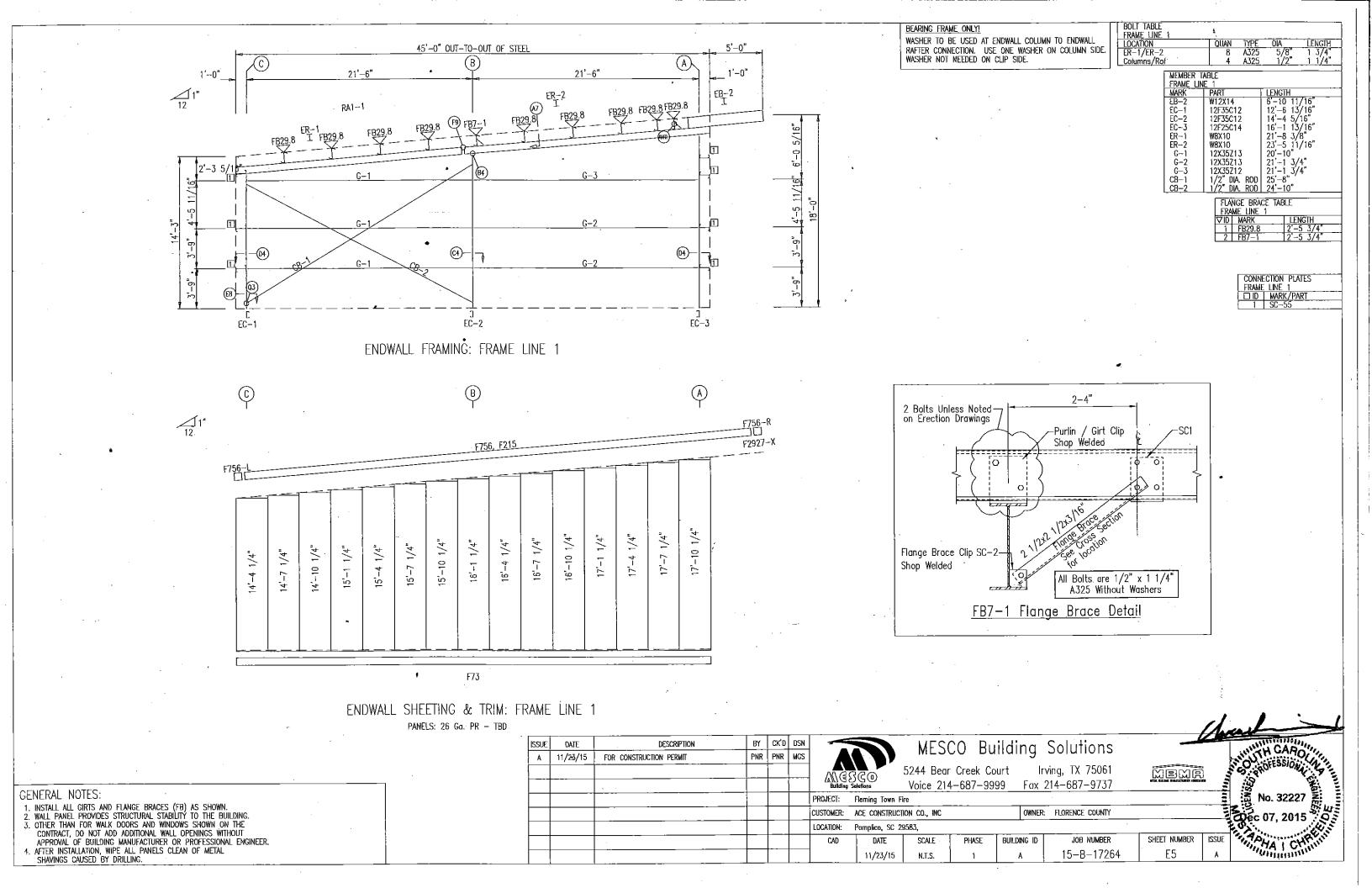
GENERAL NOTES:
1. INSTALL ALL PURLIN AND FLANGE BRACES (FB) AS SHOWN.
2. ROOF PANEL PROVIDES STRUCTURAL STABILITY TO THE BUILDING.
3. STRUT PURLINS, IF PROVIDED, MUST BE INSTALLED AND FASTENED TO ROOF SHEETING PER "PBR" PANEL ROOF DETAIL
4. DO NOT ADD ANY ADDITIONAL ROOF OPENINGS WITHOUT BUILDING MANUFACTURER APPROVAL OR PROFESSIONAL ENGINEER APPROVAL.
5. DO NOT STACK SHEET BUNDLES ON ROOF, ONLY RAISE INDIVIDUAL SHEETIS AS NEEDED.
6. AFTER INSTALLATION, WIPE ALL PANELS CLEAN OF METAL SHAVINGS CAUSED BY ORILLING.

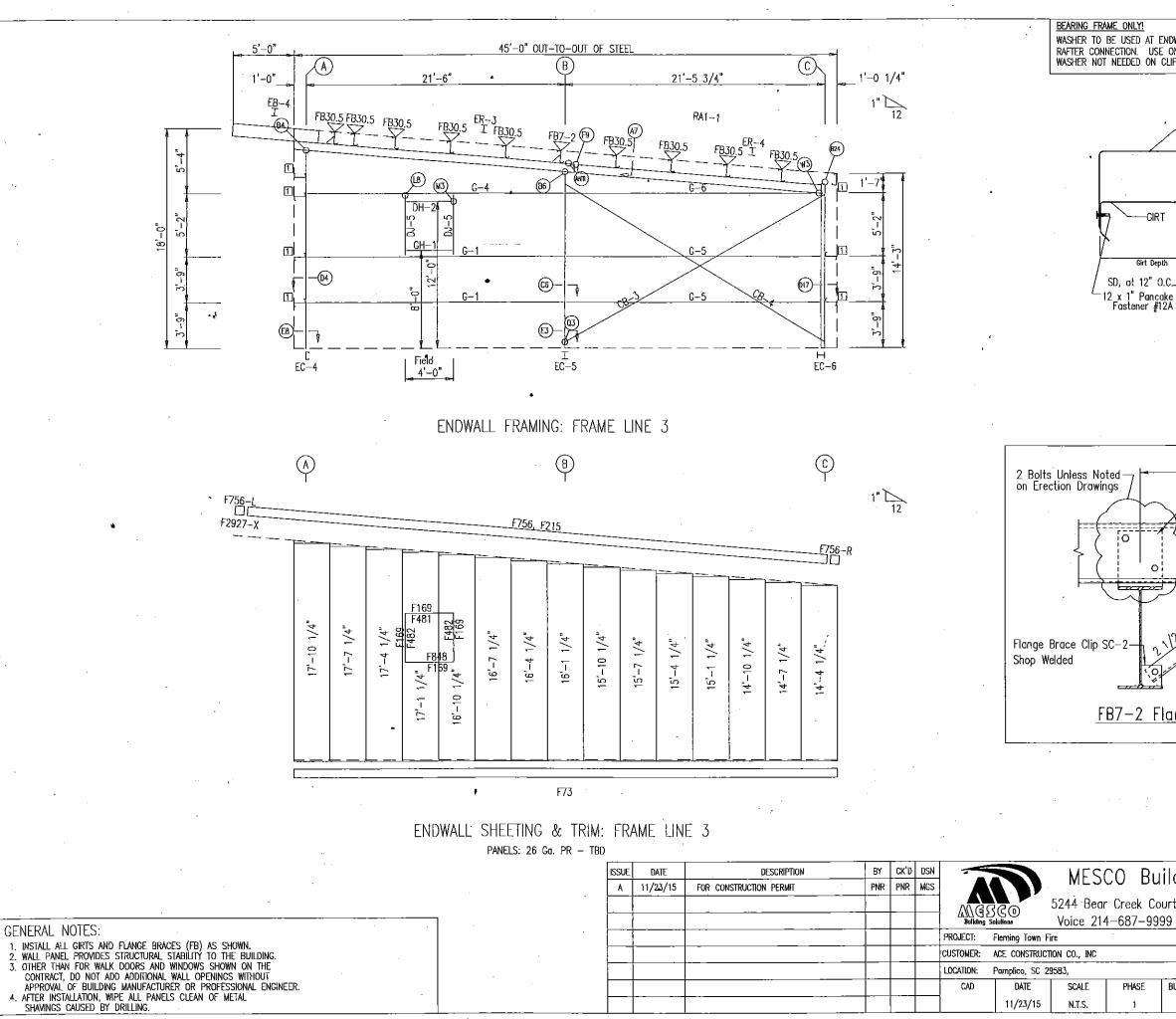
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OWNER: FLORENCE CO	UNTY		5 07 004F	\$ 55
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JILDING ID JOB NUX	MBER SHEE	t number issue E2 a	CUEC 07, 2015	



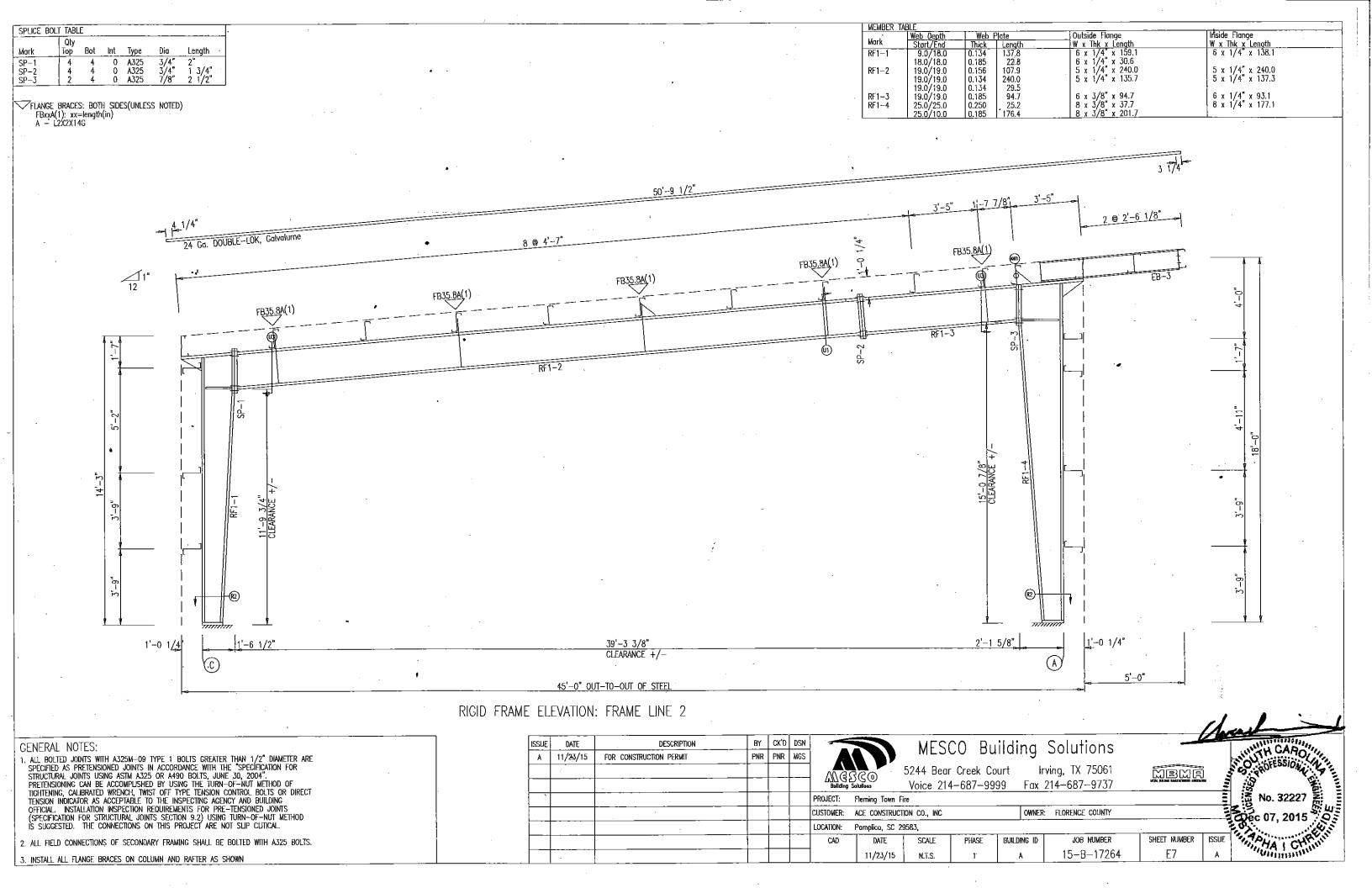


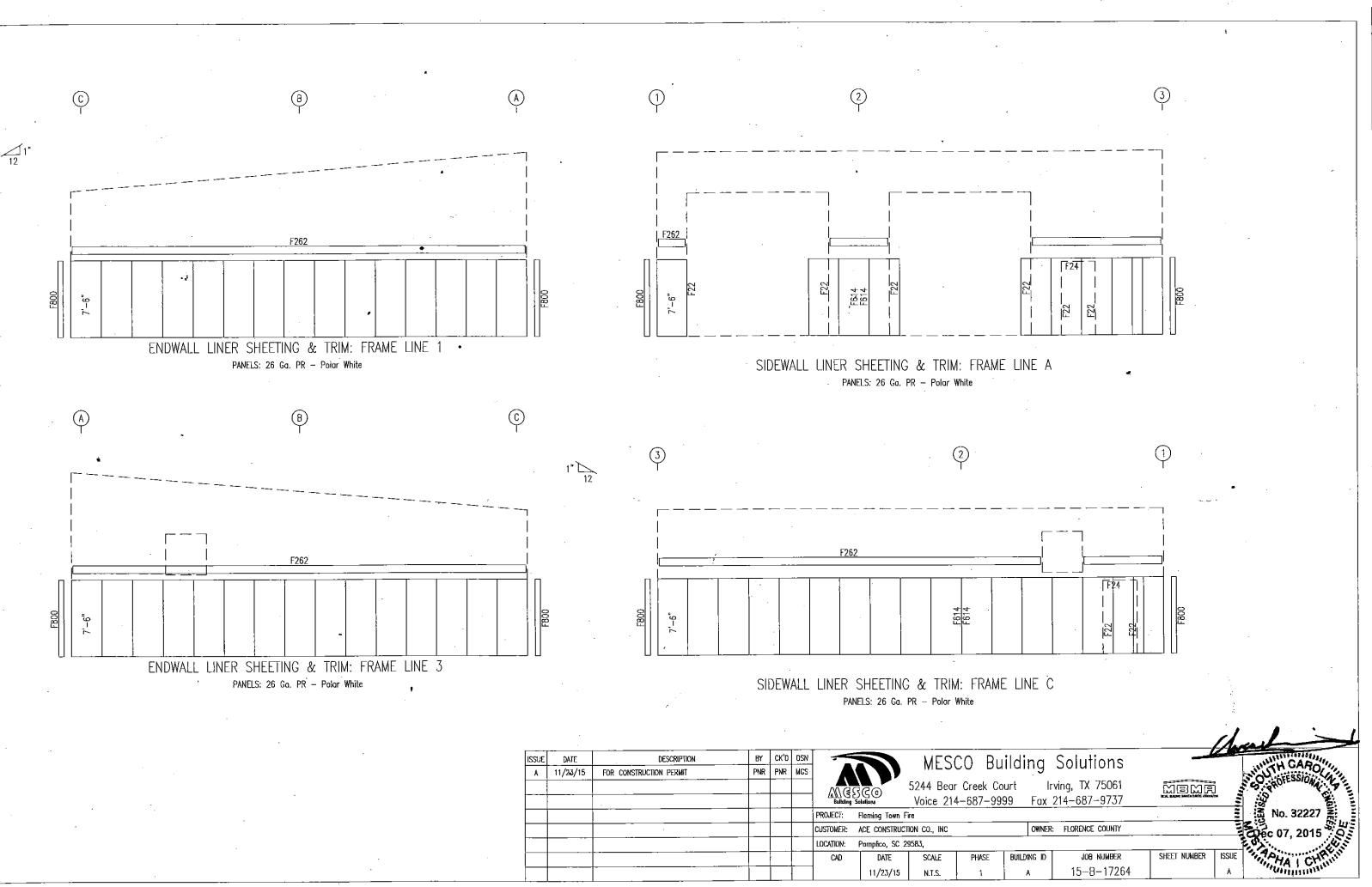
15-B-17264 E4 A



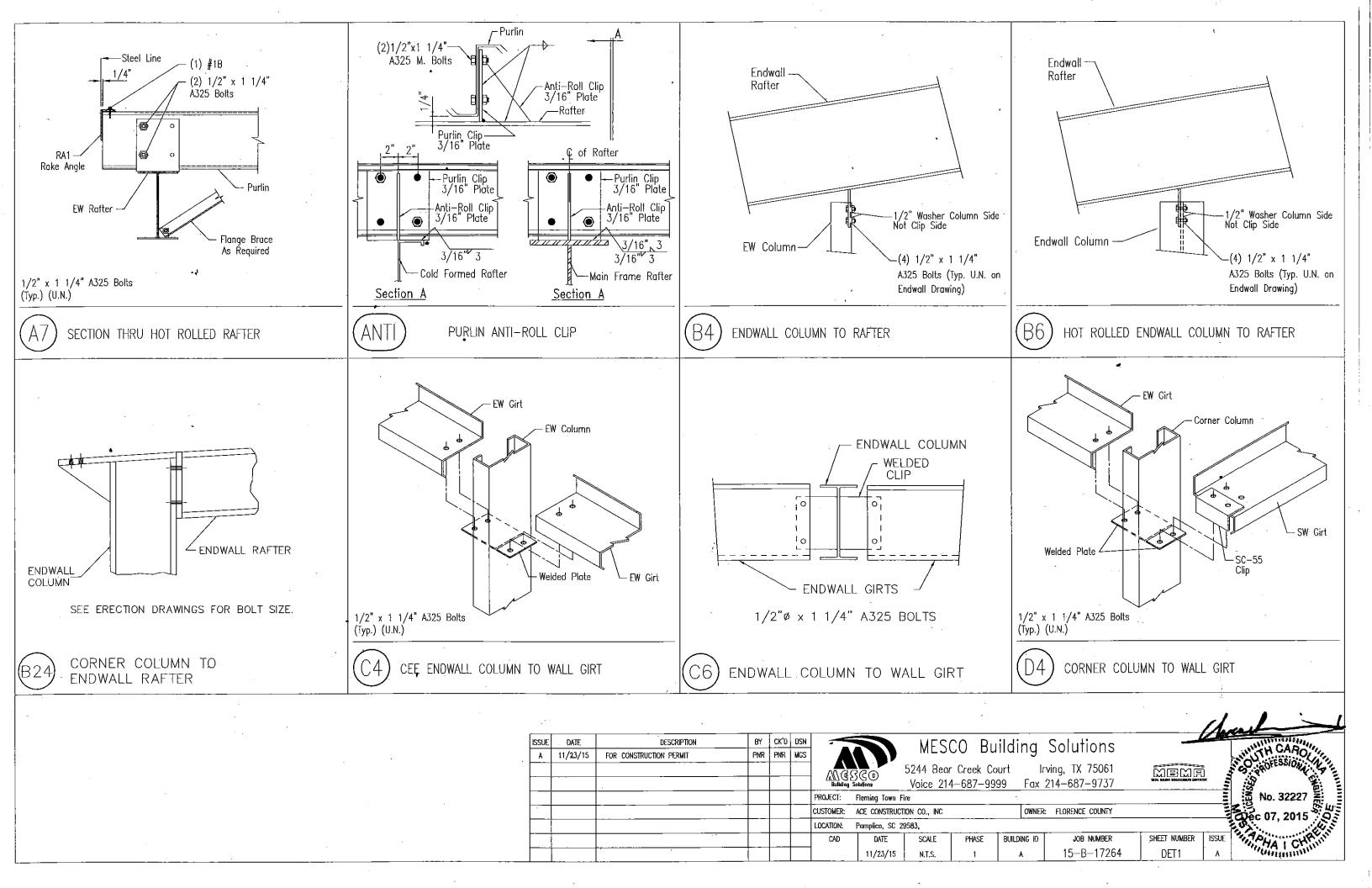


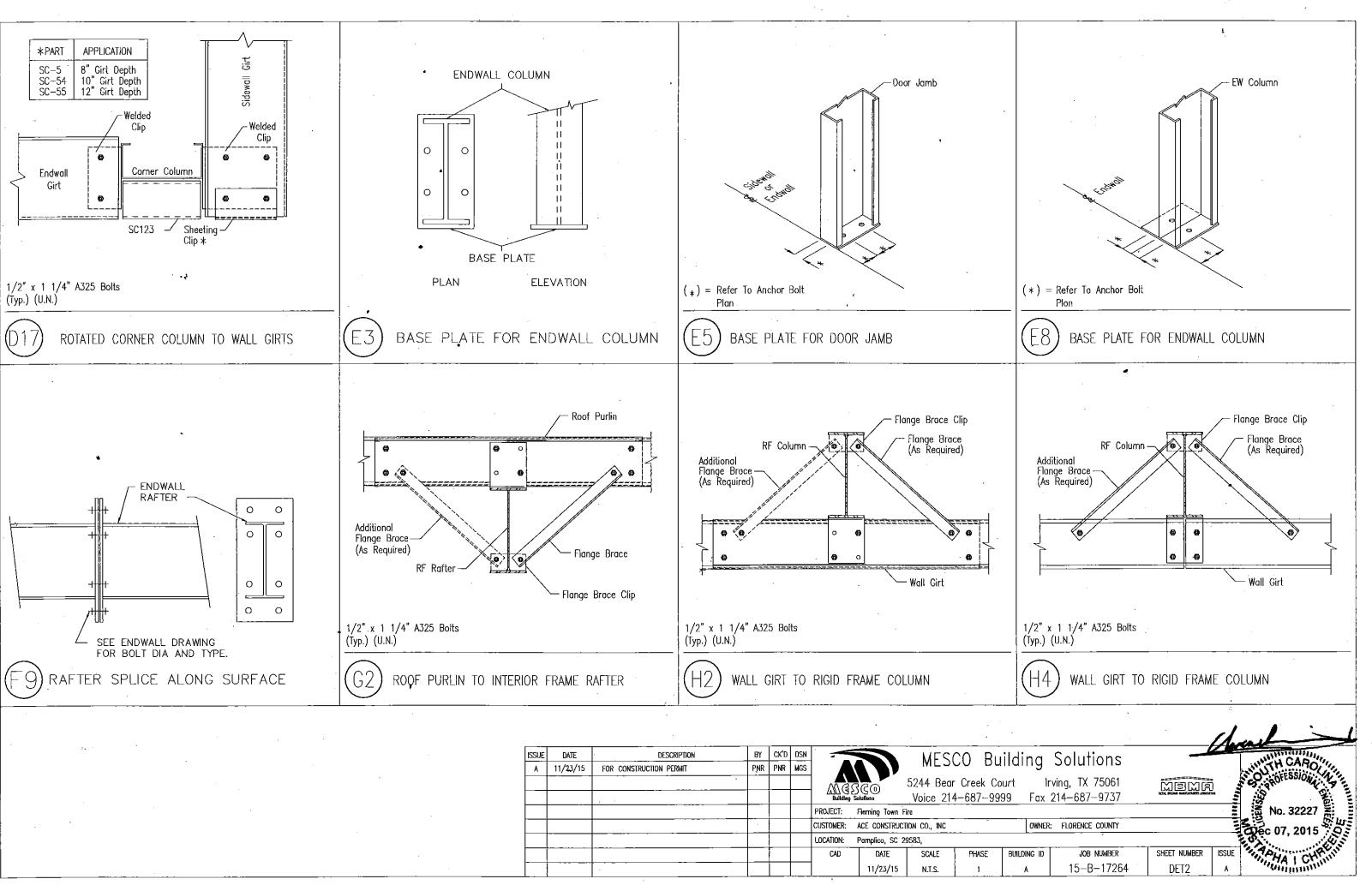
DWALL COLUMN TO ENDWALL	BOLT TABLE FRAME_LINE_3 LOCATION		TYPE DIA	LENGTH
ONE WASHER ON COLUMN SIDE. IP SIDE.	EC-6/ER-4 ER-3/ER-4 EC-4/ER-3	4 8	A325 5/8"	1 1/4" 1 3/4" 1 1/4"
-	<u> </u>	4	A325 5/8" A325 1/2" A325 1/2"	1 1/4" 1 1 <u>/</u> 4"
	FR	:Mber Table : <u>Ame Line 3</u> 	LENGTH	
, GH−1	EE	3-4 W12X14 2-4 12F25C1	6'-10 11 4 15'-11 1	/16" 3/16"
	EC	X=5         W12X14           X=6         W12X14           X=3         W10X12	14'-2 5/ 13'-4 3/	16" 4" /16"
	EF	R=4 W10X12 I=5 12F35C1	4   19'-8 9/ 4   5'-2"	16"
	DH GH	I-2   12F35C1 I-1   GH-1	4 4'-0" 4'-0"	
	(	G-1 12X35Z1 G-4 12X35Z1 G-5 12X35Z1	$\begin{array}{cccc} 2 & 20'-10'' \\ 3 & 20'-1.9/ \end{array}$	16"
<del></del>	CE	6   12X35Z1 3-3   1/2" DIA	3   18'-11 5 ROD   23'-11"	/8"
; e		<u>1/2" DIA</u> FLANC	. ROD   24°-9° GE BRACE TABLE	
e Å		FRAM. ▽ID	<u>e line 3</u> Mark lep	IGTH
			FB30.5 2'- FB7-2 2'-	6 <u>1/2"</u> 6 1/2"
	•		CONNECTION PLA	TES
			FRAME LINE 3	RT
	,	I	1 SC-55	
	• 	Т		
2-4"		}		
Durlin / Oist Olis	_001			
Purlin / Girt Clip Shop Welded	-SC1			
	≥ o	•		
1.5°				
1215 Brock Section.				
2x2 Flore Crossion				
All Bolts are 1/2" x	1 1/4"			
All Boits are 1/2 X A325 Without Was	hers			
<u>ange Brace Detail</u>				
	-	1	1	(
Iding Solutions		And	A CAN	441.
rt Irving, TX 75061	<b></b>		C LOFESSION	Lin 4
Fax 214–687–9737			3	
OWNER: FLORENCE COUNTY		N	No. 3222	S LU E
			Déc 07, 201	5 0 5
BUILDING ID JOB NUMBER A 15-B-1726	SHEET NU	MBER ISSUE	HA I C	HP. III
	<u>,                                     </u>		11 ji 13 i 4.	



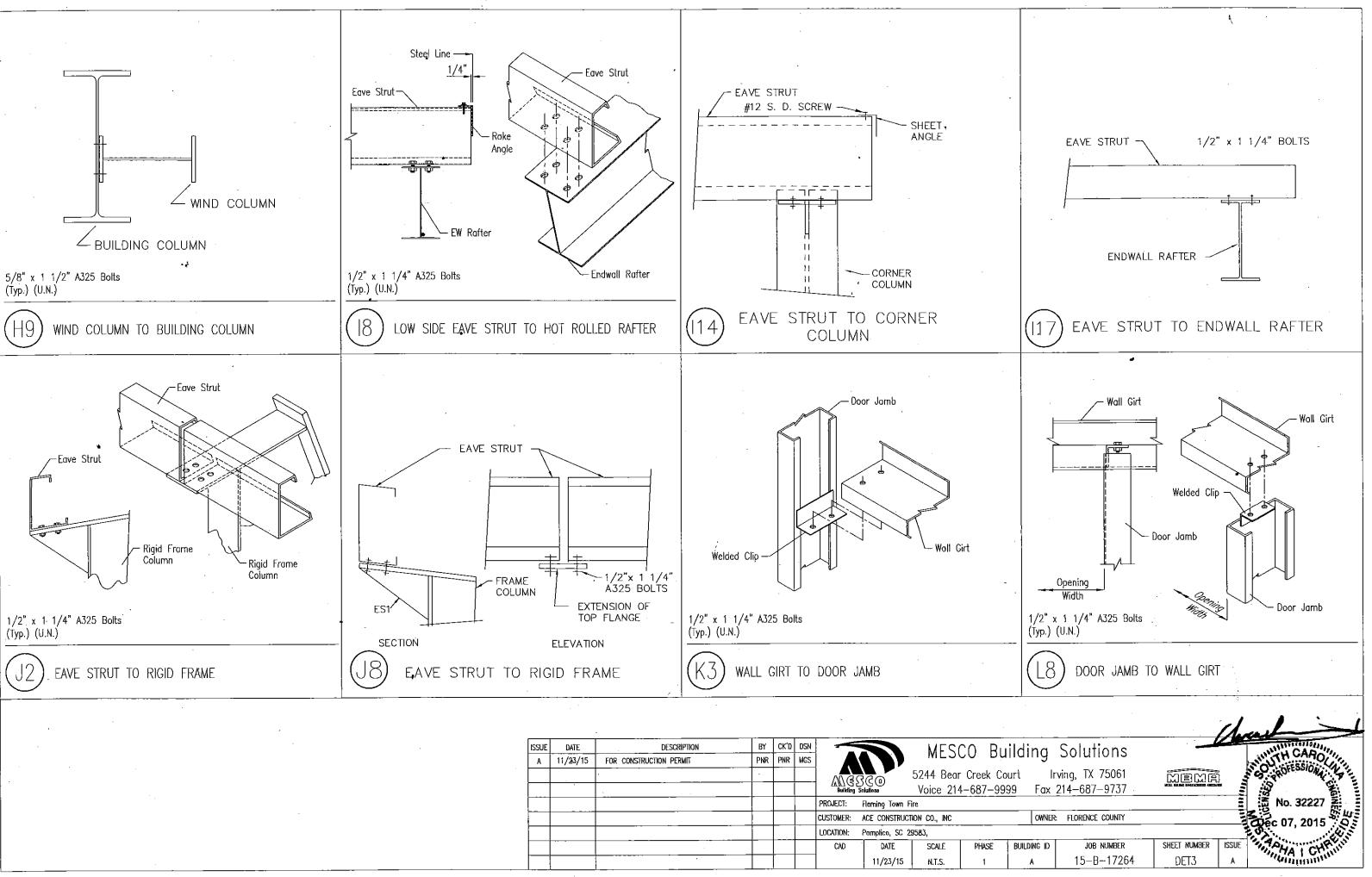


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ISSUE	DATE	DESCRIPTION	BY	ск'о	DSN			MES	CO Bi	iildi
A	11/23/15	FOR CONSTRUCTION PERMIT	PNR	PNR	MGS			NIL J		inu
			-	_ ·				5244 Bear	- Creek C	ourt
		· · · · · · · · · · · · · · · · · · ·					S(G(0) Solutions		4–687–99	
						PROJECT:	Fleming Town F	îre		
						CUSTOMER:	ACE CONSTRUC	TION CO., INC	_	
				1	1	LOCATION:	Pamplico, SC 2	9583,		
	· · ·	· · · · · · · · · · · · · · · · · · ·			[·	CAD	DATE	SCALE	PHASE	BUIL
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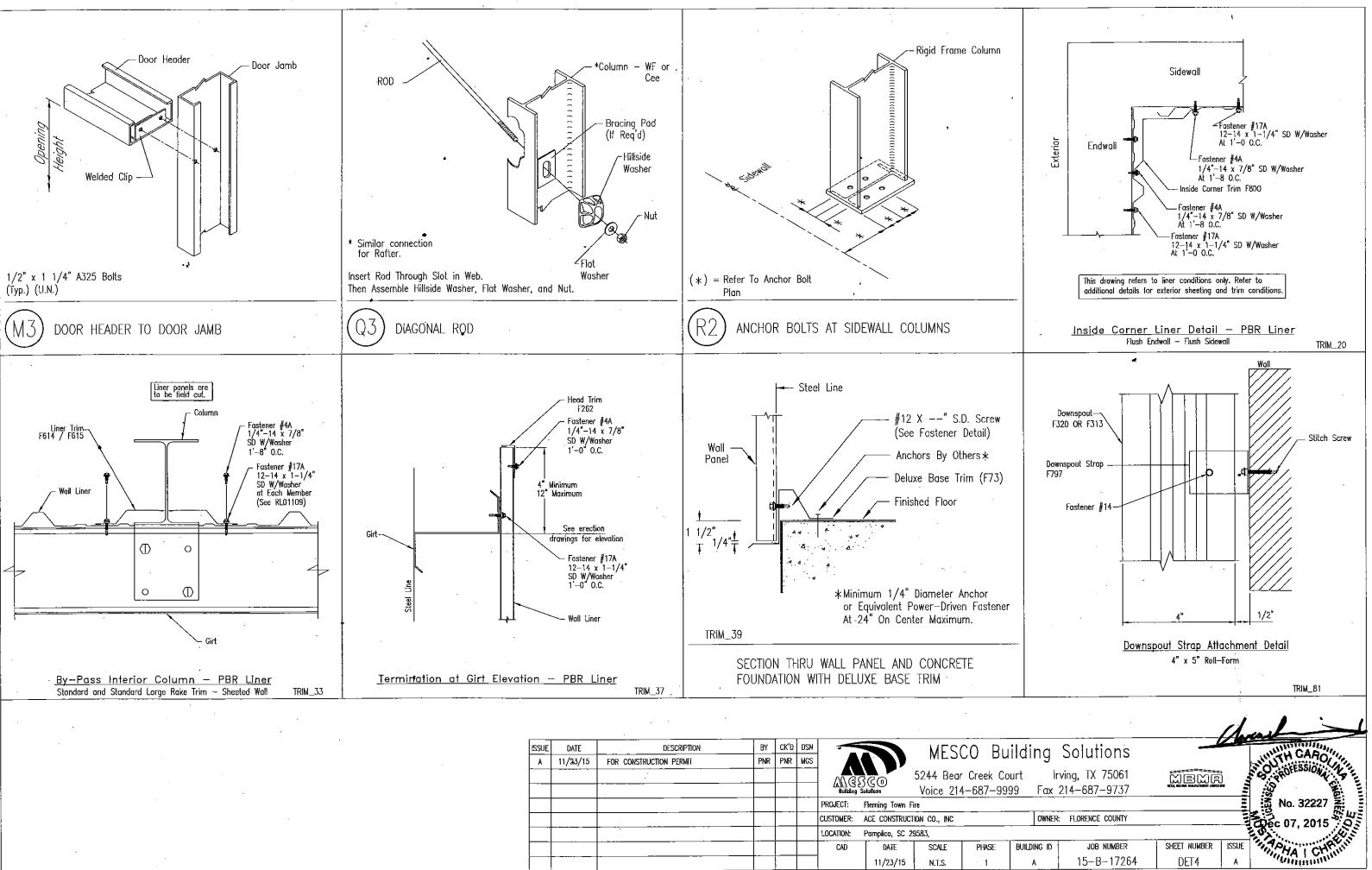




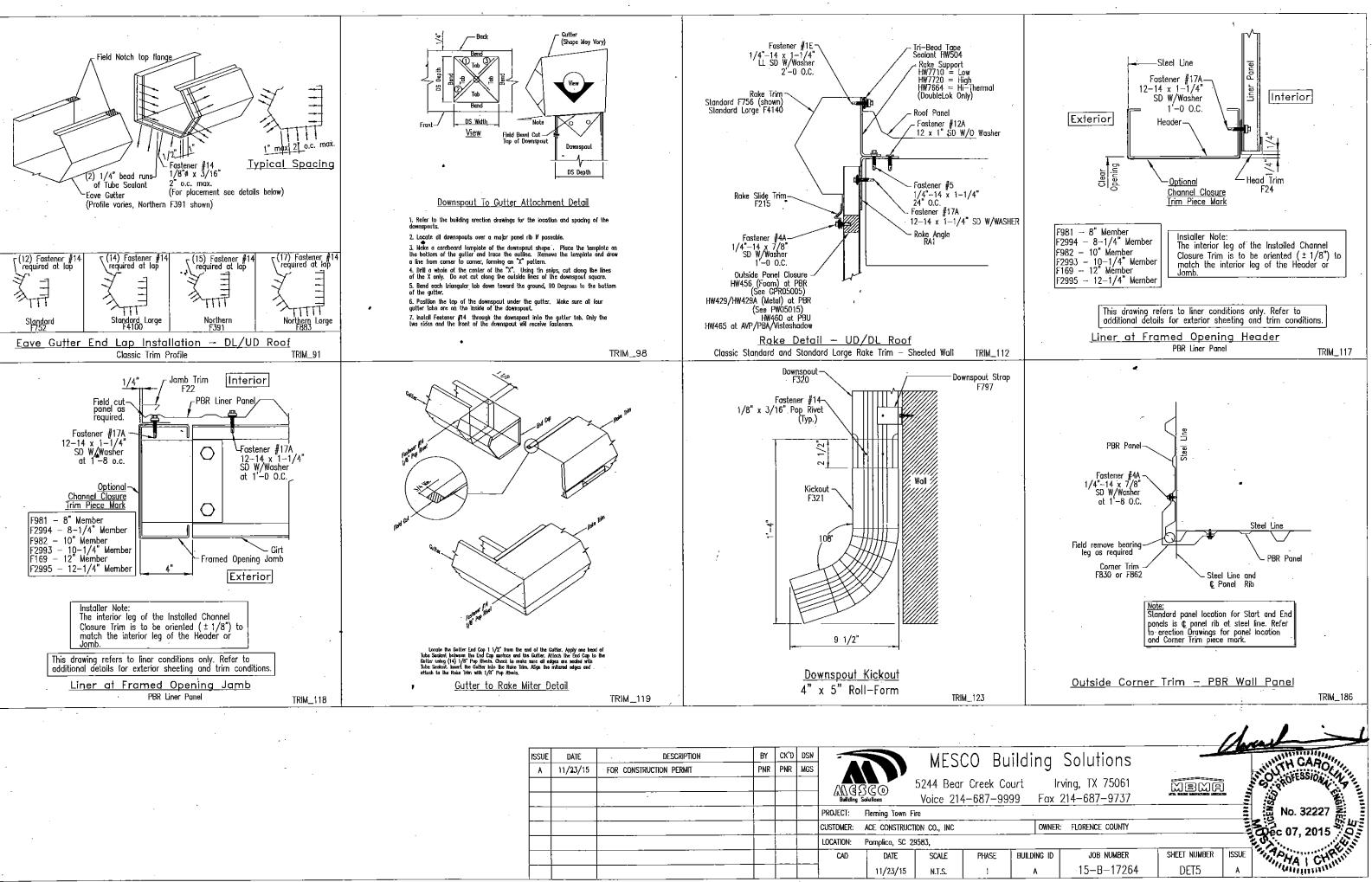
ISSUE	DATE	DESCRIPTION	BY	CK'D	DSN	·		MESO	CO Bu	uldir
A	11/23/15	For Construction Permit	P <u>N</u> R	PNR	MGS				00 00	mun
							760	5244 Bear	<sup>-</sup> Creek Co	ourt
		· · ·		1		Building	Solutions	Voice 214	4–687–99	99
						PROJECT:	Fleming Town F	ire		
			<u> </u>			CUSTOMER:	ACE CONSTRUCT	TION CO., INC		
				}		LOCATION:	Pamplico, SC 2	9583,		
				T		CAD	DATE	SCALE	PHASE	BUILDIN
		•					11/23/15	N.T.S.	1	A



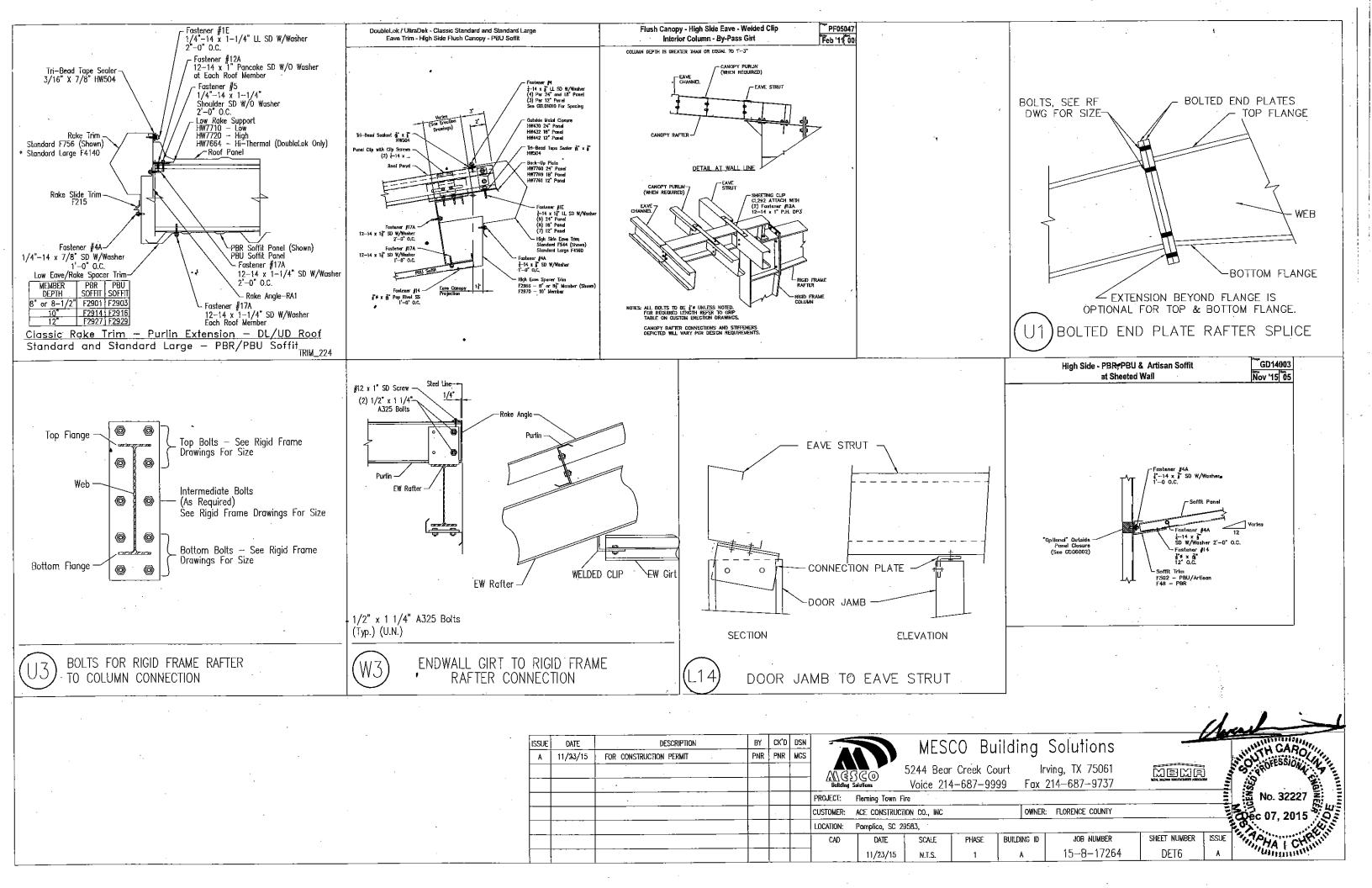
				-		<u> </u>	Ra	5244 Bea	с сгеек со	iU
	'					Building So	dutions	Voice 21	4-687-99	9
				[		Project: (	Fleming Town F	ìre		
i			 _			CUSTOMER: /	ACE CONSTRUC	Ron Co., Inc		
						Location: {	Pamplico, SC 2	9583,		
		_				CAD	DATE	SCALE	PHASE	ſ
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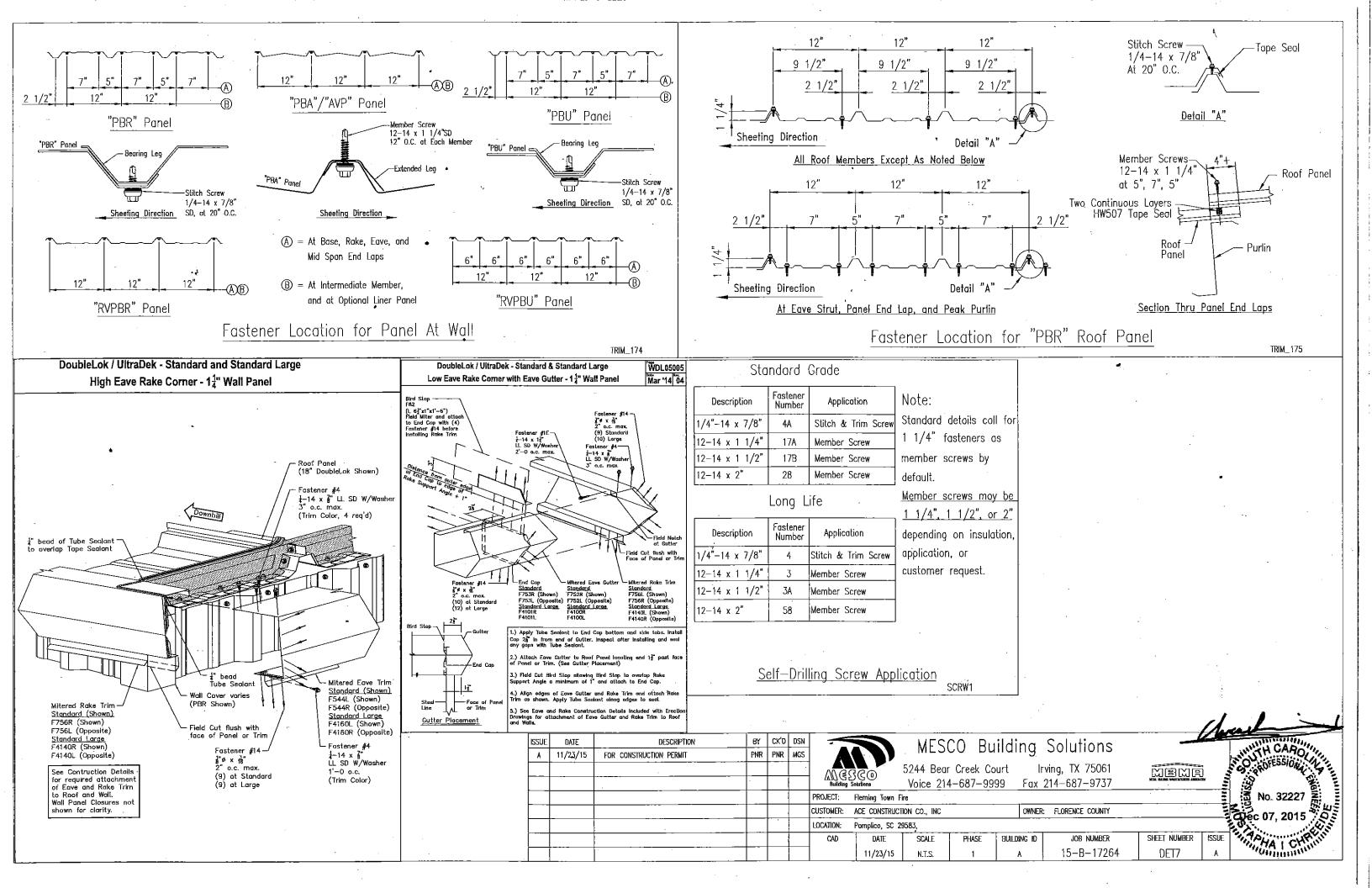


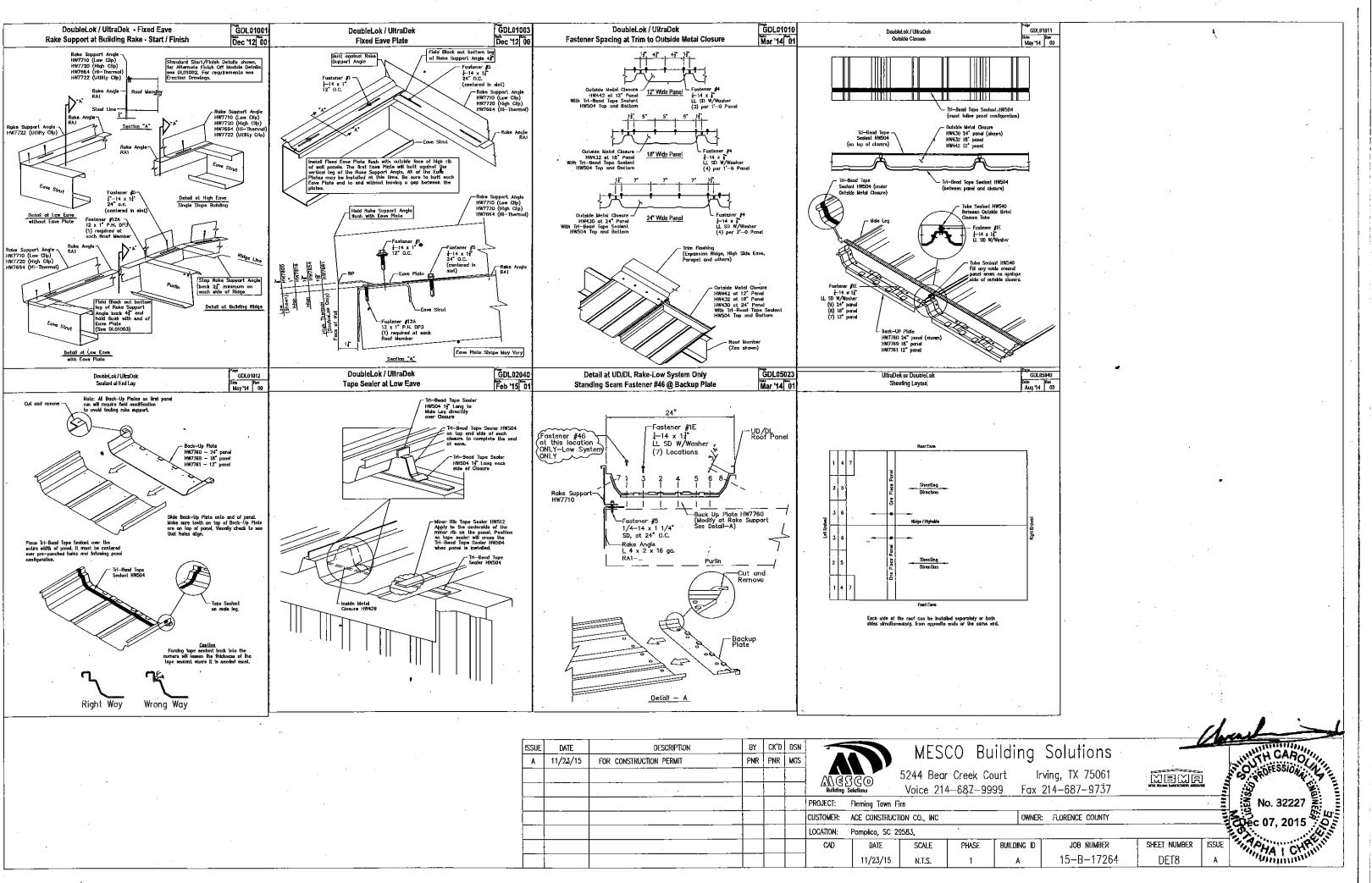
ISSUE	DATE	DESCRIPTION	BY	CK'D	dsn	MESCO Bui	ГЧ
Å	11/23/15	For construction permit	PNR	PNR	MGS	WILSOU BUI	ľu
-		· · · · · · · · · · · · · · · · · · ·				ANGSCO 5244 Bear Creek Cou	
						Building Solutions Voice 214-687-9999	3
			_			PROJECT: Flerning Town Fire	
					[	CUSTOMER: ACE CONSTRUCTION CO., INC	
		····				LOCATION: Pamplico, SC 29583,	
	••					CAD DATE SCALE PHASE	BUIL
					İ	11/23/15 N.T.S. 1	



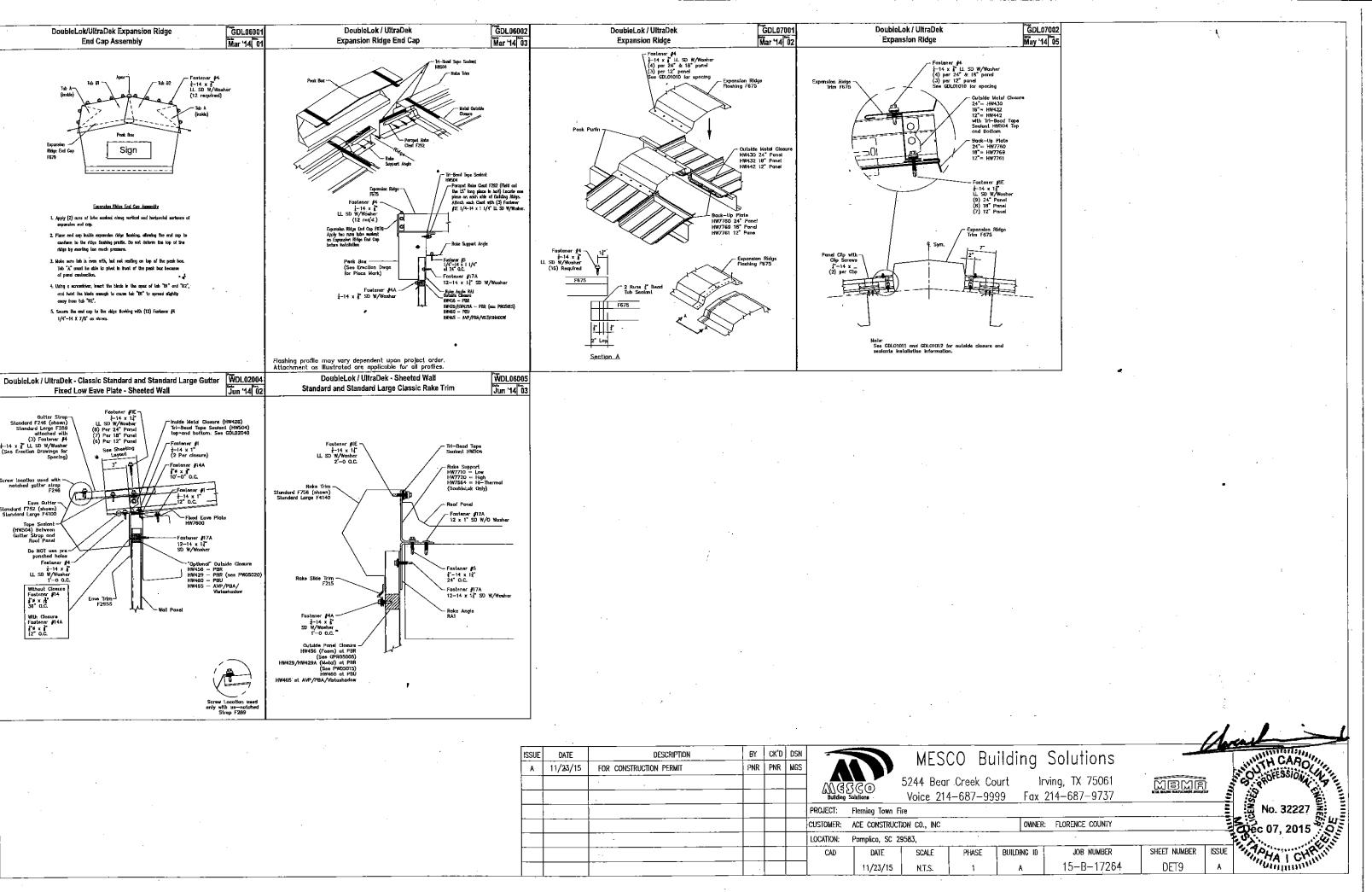
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ISSUE	DATE	- DESCRIPTION	BY	כא'ם	DSN		5	MES	CO BL	uldir
A	11/23/15	FOR CONSTRUCTION PERMIT	PNR	PNR	MGS					inun
		·		[	-		CO	5244 Bea	r Creek Ci	ourt
				F		Building Sa	kellans	Voice 21	4-687-99	999
						PROJECT: I	Fleming Jown I	-ìre		
				1		CUSTOMER:	ACE CONSTRUC	TION CO., INC		
					ļ	LOCATION: I	Pomplico, SC 2	29583,		
						CAD	DATE	SCALE	PHASE	BUILDIN
					<u>                                      </u>	1	11/23/15	N.T.S.	1	A

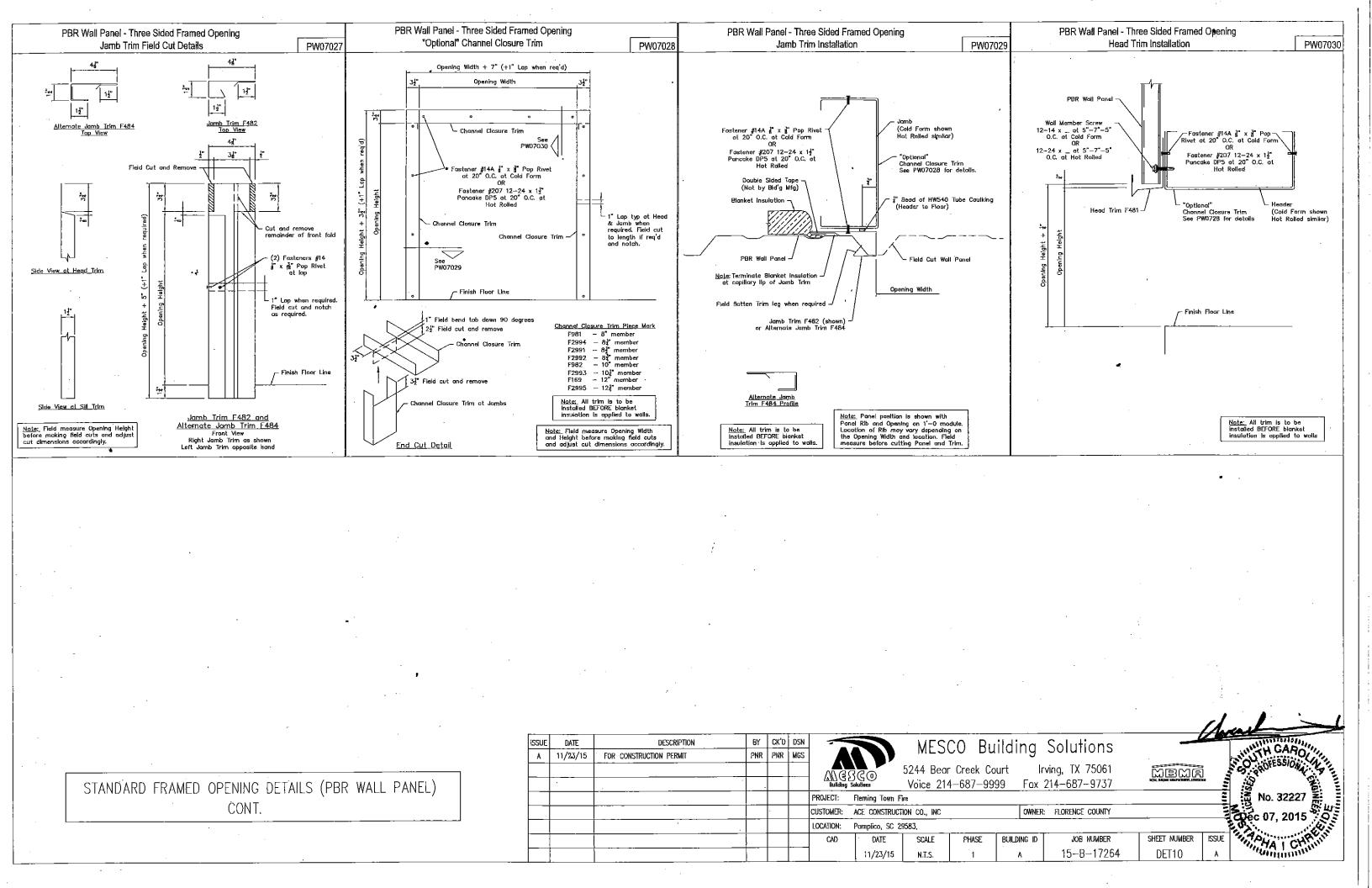


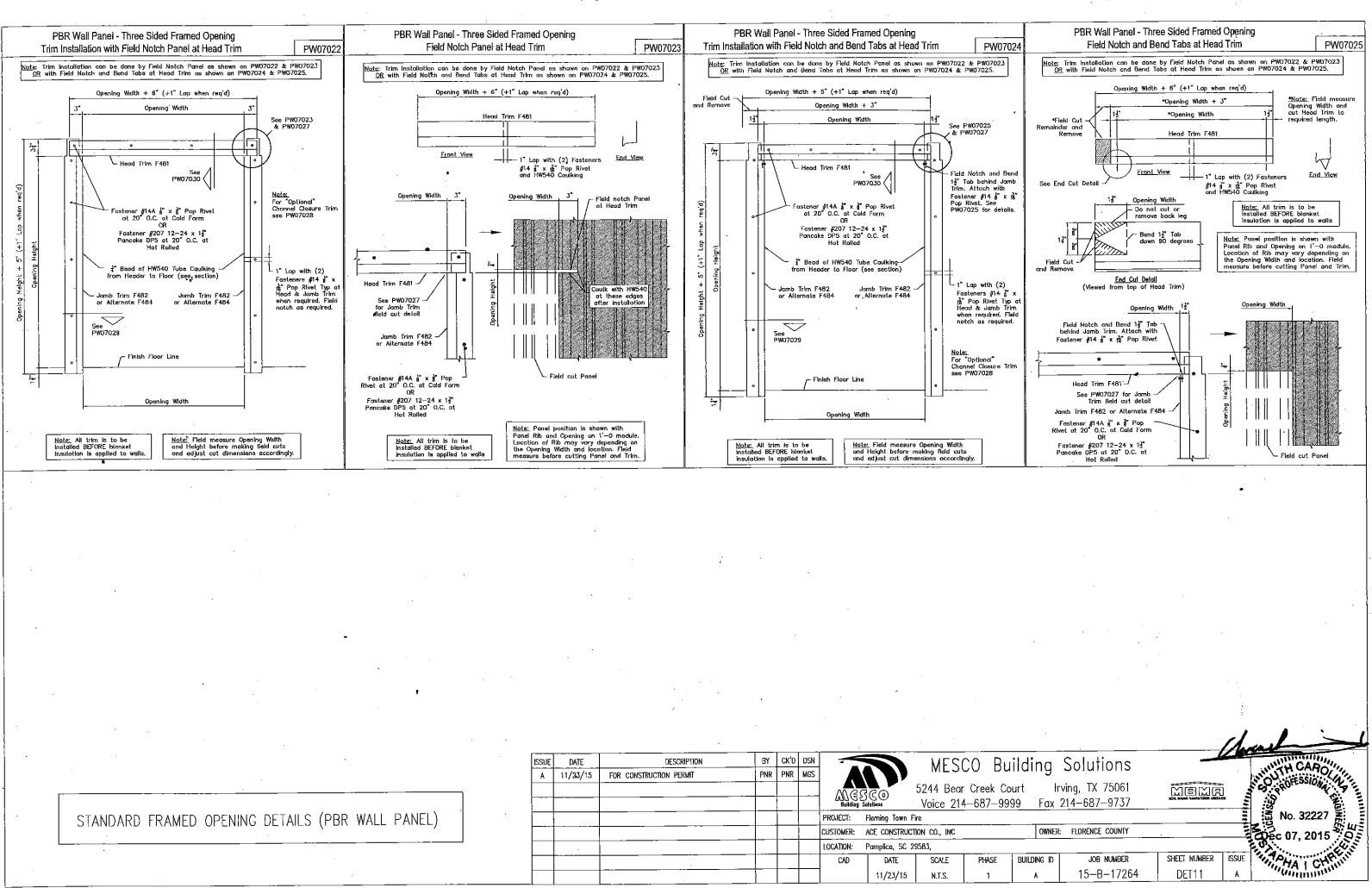




ISSUE	DATE	DESCRIPTION	8Y	CK,D	DSN			MES	CO B	uildin
A	11/23/15	FOR CONSTRUCTION PERMIT	PNR	PNR	MGS			NLJ		unun
					ļ		360	5244 Bea	r Creek C	ourt
					}	Euliding	Solutions	Voice 21	4-687-9	999 I
						PROJECT:	Fleming Town I	 Fire	-	
						CUSTOMER:	ACE CONSTRUC	tion co., inc		(
				T		LOCATION:	Pamplico, SC 2	29583,		
						CAD	DATE	SCALE	PHASE	BUILDIN
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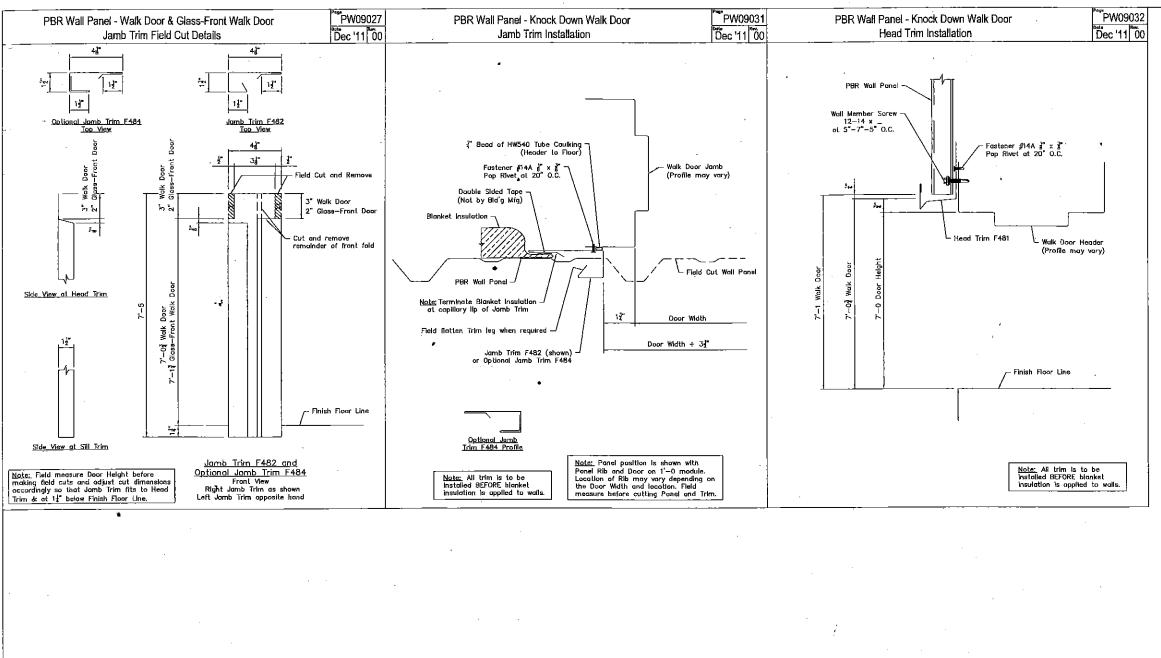






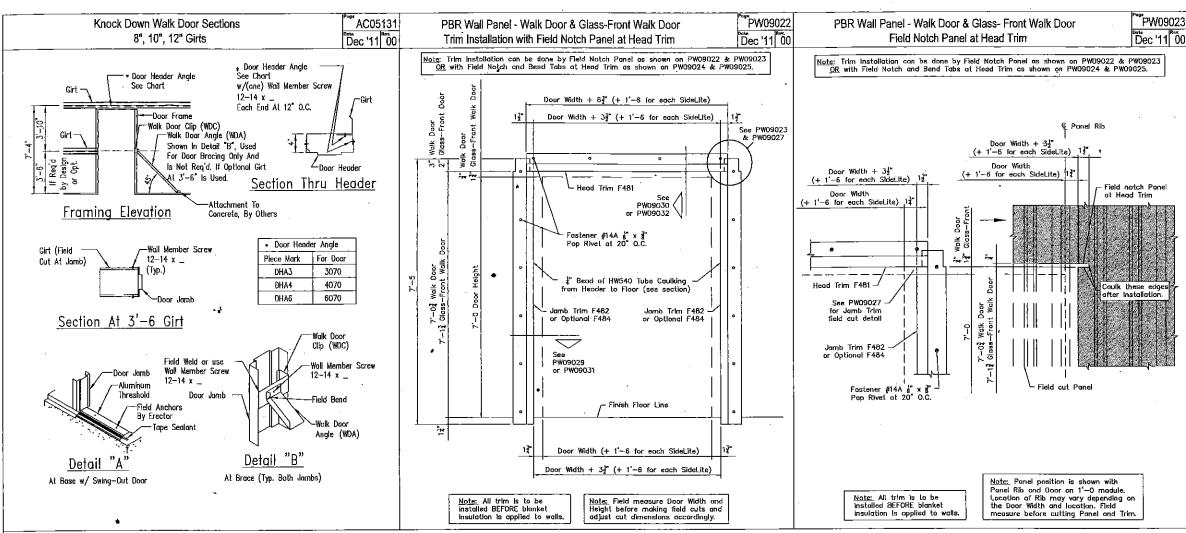
STANDARD FRAM	IED OPENING	DETAILS	(PBR	WALL	PANEL)	)
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A	11/23/15	FOR CONSTRUCTION PERMIT	PNR	PNR	MGS			NILS		mun
	,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,						260	5244 Bea	r Creek Co	ourt
							Satutions	Voice 21	4–687–99	99
						PROJECT:	Fleming Town Fi	re		
<u> </u>						CUSTOMER:	ACE CONSTRUCT	ION CO., INC		
					1	LOCATION:	Pamplica, SC 2	9583		
						CAD	DATE	SCALE	PHASE	BUILDI
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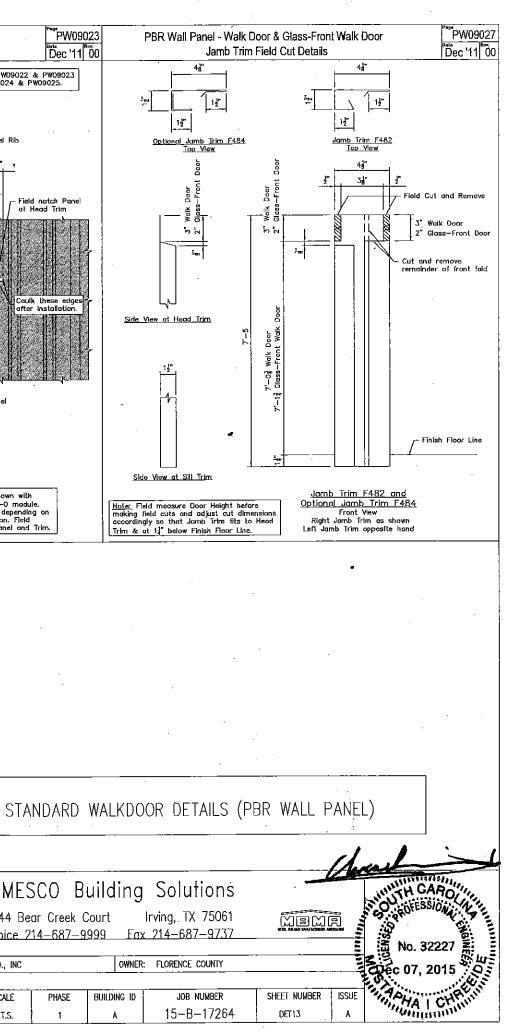


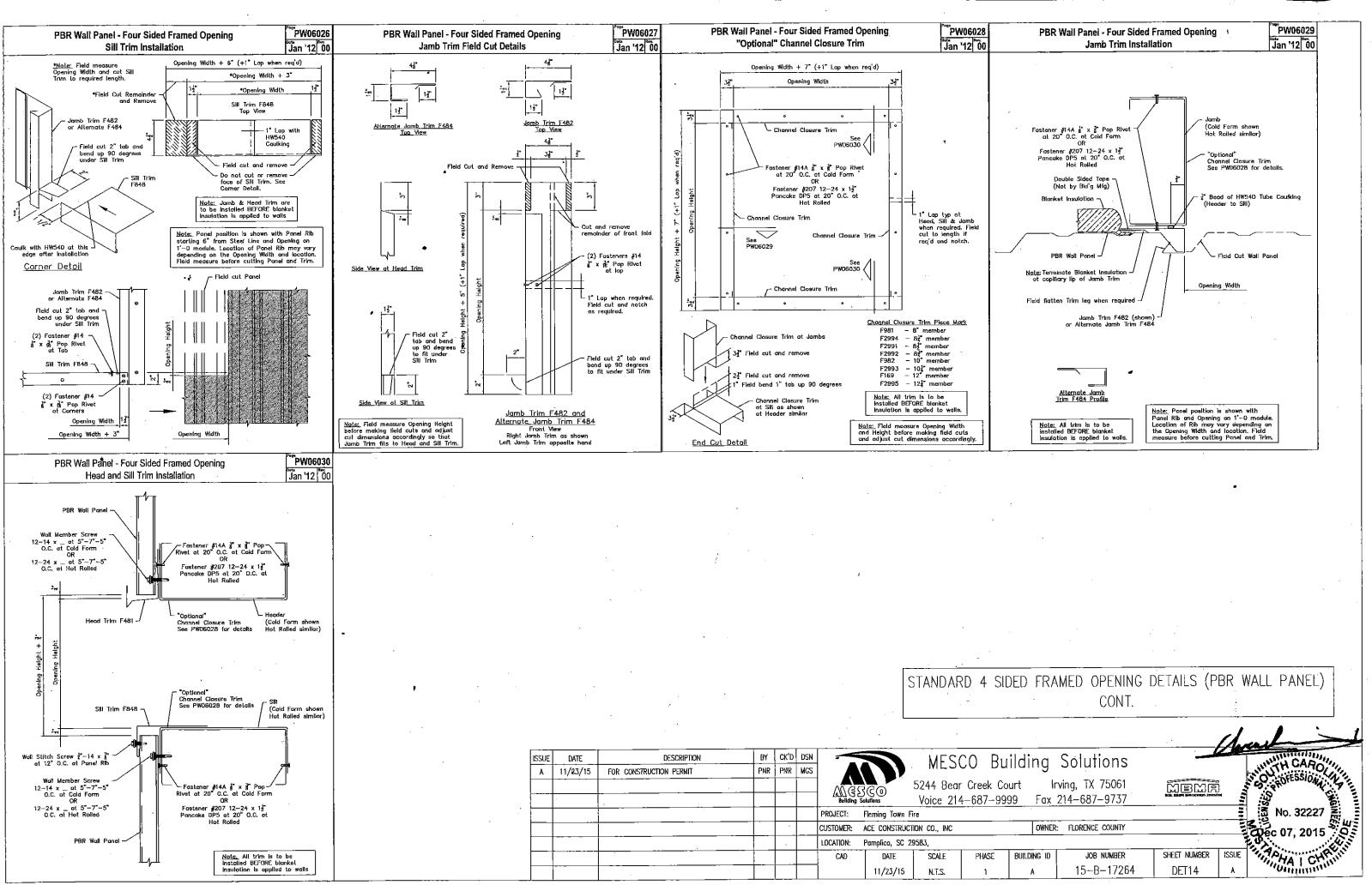
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			·			·								
							,	STA	NDARD	WALKDO	OR DETAILS (P CONT.	BR WALL F	PANEL	_)
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T		· · · · · · · · · · · · · · · · · · ·	-		<u> </u>								An	ast
isue A	DATE 11/23/15	DESCRIPTION FOR CONSTRUCTION PERMIT	BY PNR	_	DSN Mgş			MES	CO Bl	uilding	Solutions			WITH CARO
			-				SCO Solutions	5244 Bea		ourt li	rving, TX 75061 214—687—9737			CO TOFESSIONAL MAL
+			-			PROJECT:	Fleming Town							No. 32227
						CUSTOMER:	ACE CONSTRUC			OWNER	R: FLORENCE COUNTY			Qec 07, 2015
		· · · · · · · · · · · · · · · · · · ·	_	-	ļ	LOCATION:	Pamplico, SC		-					
-				-	<u> </u>	CAD .	DATE	SCALE	PHASE	BUILDING ID	job number 15-B-17264	SHEET NUMBER DET12	ISSUE	MA CHINN
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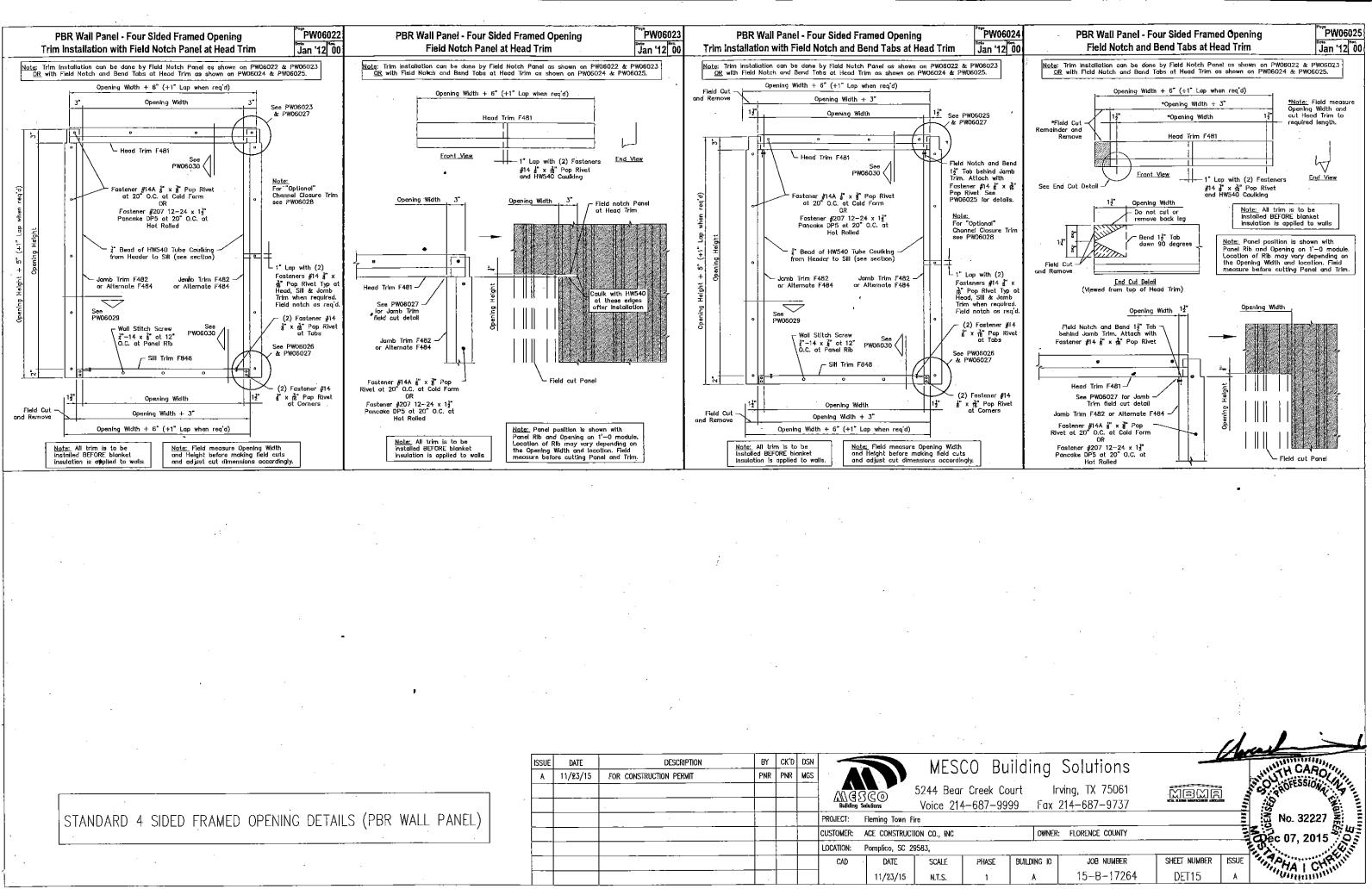


ISSUE	DATE	DESCRIPTION	BY	CK*D	DSN				SCO I	ل البر
A	11/23/15	FOR CONSTRUCTION PERMIT	PNR	PNR	MGS			NI E.	200 1	Sullu
							ICCO	5244 Be	ear Creek	Court
		-						Voice 2	14-687-	9999
				ĺ		PROJECT:	Fleming Town Fi	re		
-						CUSTOMER:	ACE CONSTRUCT	ion co., inc		
						LOCATION:	Pamplico, SC 29	9583,		
					1	CAD	DATE	SCALE	PHASE	BUILD
						1	11/23/15	N.T.S.	1	1





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SSUE	DATE	DESCRIPTION	BY	CK'D	DSN		MES	CO Bi	uİdir
A	11/23/15	FOR CONSTRUCTION PERMIT	PNR	PNR	MGS		IVIL J		unun.
						WERCO	5244 Bec	r Creek C	ourt
						Building Solutions	Voice 21	4-687-99	999
						PROJECT: Fleming Tow	n Fire		
						CUSTOMER: ACE CONST	RUCTION CO., INC		
						LOCATION: Pomplico, S	C 29583,		
						CAD DATE	SCALE	PHASE	BUILDIN
				ĺ		11/23/1	5 N.T.S.	1	A